

POLITECHNIKA POZNAŃSKA
INSTYTUT KONSTRUKCJI BUDOWLANYCH
Zakład Mechaniki Budowli

ĆWICZENIE nr 2

OBLICZANIE RAMY METODĄ PRZEMIESZCZEŃ

Prowadzący: **mgr inż. A. Kaczor**

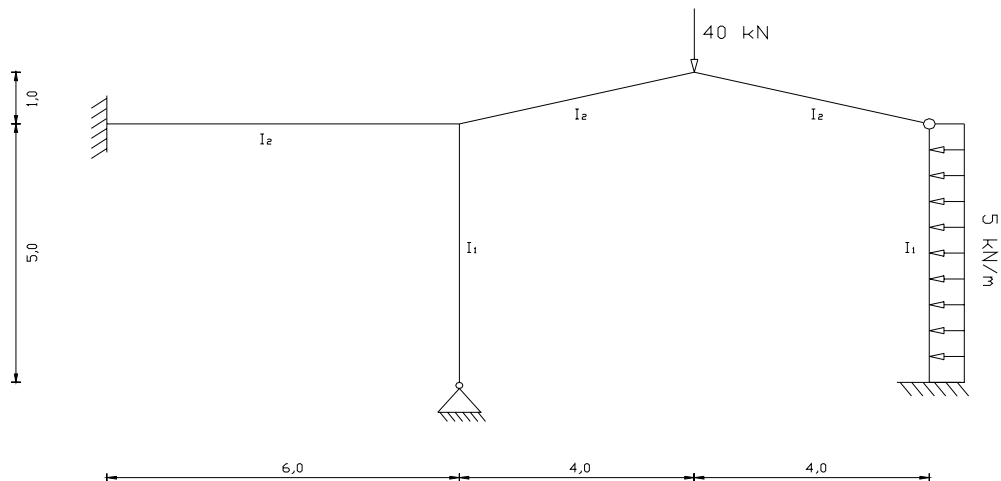
Wykonał: **Piotr Matysiak**

Grupa 1

Rok akad. 2003/2004

STUDIUM ZAOCZNE

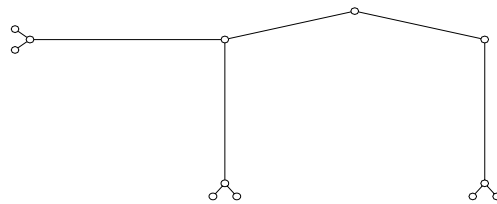
2. Schemat konstrukcji.



3. Stopień geometrycznej niewyznaczalności układu.

$SGN = \sum \Delta + \sum \varphi$, gdzie: $\sum \Delta$ – łączna liczba niezależnych przesuńczeń węzłów,
 $\sum \varphi$ – łączna liczba obrotów węzłów sztywnych

3.1. Określenie liczby przesuńczeń węzłów – łańcuch kinematyczny:

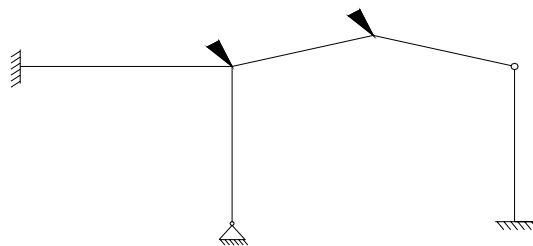


$$\sum \Delta = 2 \cdot w - p, \quad \text{gdzie: } w - \text{liczba węzłów; } w = 6$$

$$p - \text{liczba prętów; } p = 11$$

$$\sum \Delta = 2 \cdot 6 - 11 = 1$$

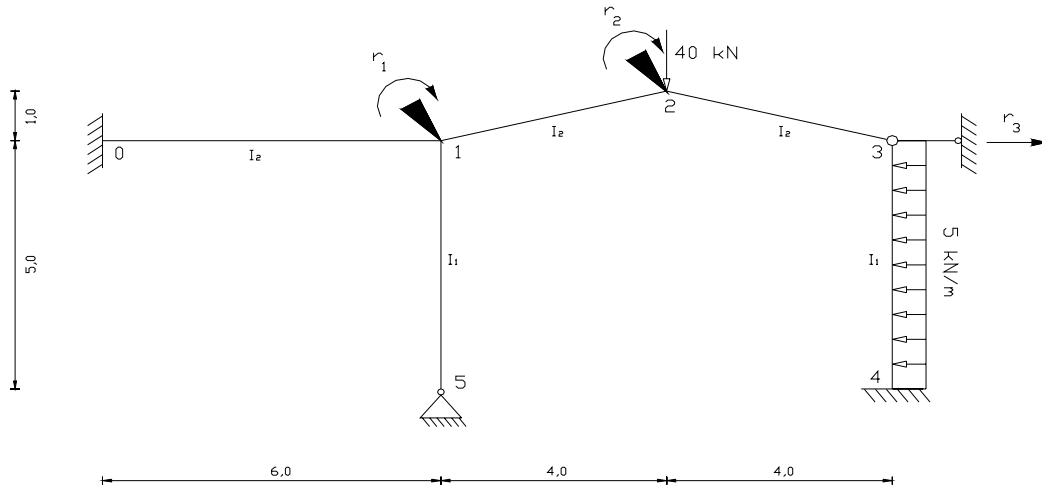
3.2. Określenie liczby obrotów węzłów sztywnych:



$$\sum \varphi = 2$$

$SGN = 1 + 2 = 3$

3.3. Układ podstawowy:



3.4. Układ równań kanonicznych:

$$\begin{aligned} r_{11} \cdot z_1 + r_{12} \cdot z_2 + r_{13} \cdot z_3 + r_{1P} &= 0 \\ r_{21} \cdot z_1 + r_{22} \cdot z_2 + r_{23} \cdot z_3 + r_{2P} &= 0 \\ r_{31} \cdot z_1 + r_{32} \cdot z_2 + r_{33} \cdot z_3 + r_{3P} &= 0 \end{aligned}$$

Niewiadome: $\varphi_1, \varphi_2, \Delta_3$

Oznaczamy: $z_1 = \varphi_1$

$z_2 = \varphi_2$

$z_3 = \Delta_3$

$$\begin{aligned} r_{11} \cdot \varphi_1 + r_{12} \cdot \varphi_2 + r_{13} \cdot \Delta_3 + r_{1P} &= 0 \\ r_{21} \cdot \varphi_1 + r_{22} \cdot \varphi_2 + r_{23} \cdot \Delta_3 + r_{2P} &= 0 \\ r_{31} \cdot \varphi_1 + r_{32} \cdot \varphi_2 + r_{33} \cdot \Delta_3 + r_{3P} &= 0 \end{aligned}$$

3.5. Współczynnik porównawczy sztywności:

I_1 – dwuteownik zwykły 220 ($I_x = 3060 \text{ cm}^4$; $W = 278 \text{ cm}^3$);

I_2 – dwuteownik zwykły 260 ($I_x = 5740 \text{ cm}^4$; $W = 442 \text{ cm}^3$);

E – współczynnik sprężystości podłużnej $E = 205 \text{ GPa}$

$$EI_1 = 205 \cdot 10^9 \cdot 3060 \cdot 10^{-8} = 6273000 \text{ Nm}^2 = 6273 \text{ kNm}^2$$

$$EI_2 = 205 \cdot 10^9 \cdot 5740 \cdot 10^{-8} = 11767000 \text{ Nm}^2 = 11767 \text{ kNm}^2$$

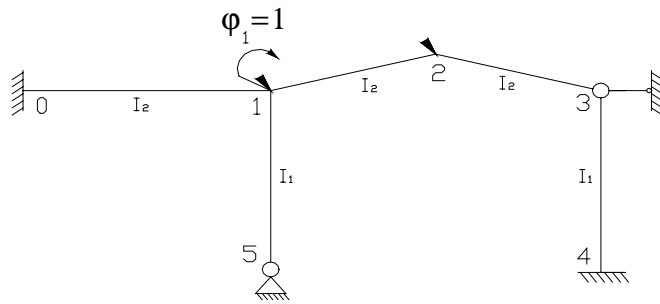
Przyjęto współczynnik porównawczy sztywności $EI_0 = EI_2$

$$EI_2 = EI_0 = 11767 \text{ kNm}^2, \quad EI_1 = 0,5331 EI_0$$

3.6. Łańcuch kinematyczny:

$$\begin{aligned} \rightarrow 015 & \quad 0 \cdot \Psi_{01} - 5 \cdot \Psi_{15} = 0 & \rightarrow \Psi_{15} = 0 \\ \uparrow 015 & \quad 6 \cdot \Psi_{01} - 0 \cdot \Psi_{15} = 0 & \rightarrow \Psi_{01} = 0 \\ \rightarrow 43 & \quad 5 \cdot \Psi_{34} = \Delta & \rightarrow \Psi_{34} = \Delta/5 \\ \uparrow 51234 & \quad 0 \cdot \Psi_{15} + 4 \cdot \Psi_{12} + 4 \cdot \Psi_{23} + 0 \cdot \Psi_{34} = 0 & \rightarrow \Psi_{12} = -\Psi_{23} \\ \rightarrow 5123 & \quad 5 \cdot \Psi_{15} + 1 \cdot \Psi_{12} - 1 \cdot \Psi_{23} = \Delta \\ & \quad 5 \cdot 0 - \Psi_{23} - \Psi_{23} = \Delta & \rightarrow \Psi_{23} = -\Delta/2 \\ & & \rightarrow \Psi_{12} = \Delta/2 \end{aligned}$$

4. Stan $\varphi_1 = 1$.



$$M_{01} = \frac{2EI_2}{l} \cdot (2 \cdot \varphi_0 + \varphi_1 - 3 \cdot \psi_{01}) = \frac{2EI_0}{6} \cdot (2 \cdot 0 + 1 - 3 \cdot 0) = \frac{1}{3} EI_0$$

$$M_{10} = \frac{2EI_2}{l} \cdot (2 \cdot \varphi_1 + \varphi_0 - 3 \cdot \psi_{01}) = \frac{2EI_0}{6} \cdot (2 \cdot 1 + 0 - 3 \cdot 0) = \frac{2}{3} EI_0$$

$$M_{15} = \frac{3EI_1}{l} \cdot (\varphi_1 - \psi_{15}) = \frac{3 \cdot 0,5331EI_0}{5} \cdot (1 - 0) = 0,31986EI_0$$

$$M_{51} = 0$$

$$M_{12} = \frac{2EI_2}{l} \cdot (2 \cdot \varphi_1 + \varphi_2 - 3 \cdot \psi_{12}) = \frac{2EI_0}{\sqrt{17}} \cdot (2 \cdot 1 + 0 - 3 \cdot 0) = 0,97014EI_0$$

$$M_{21} = \frac{2EI_2}{l} \cdot (2 \cdot \varphi_2 + \varphi_1 - 3 \cdot \psi_{12}) = \frac{2EI_0}{\sqrt{17}} \cdot (2 \cdot 0 + 1 - 3 \cdot 0) = 0,48507EI_0$$

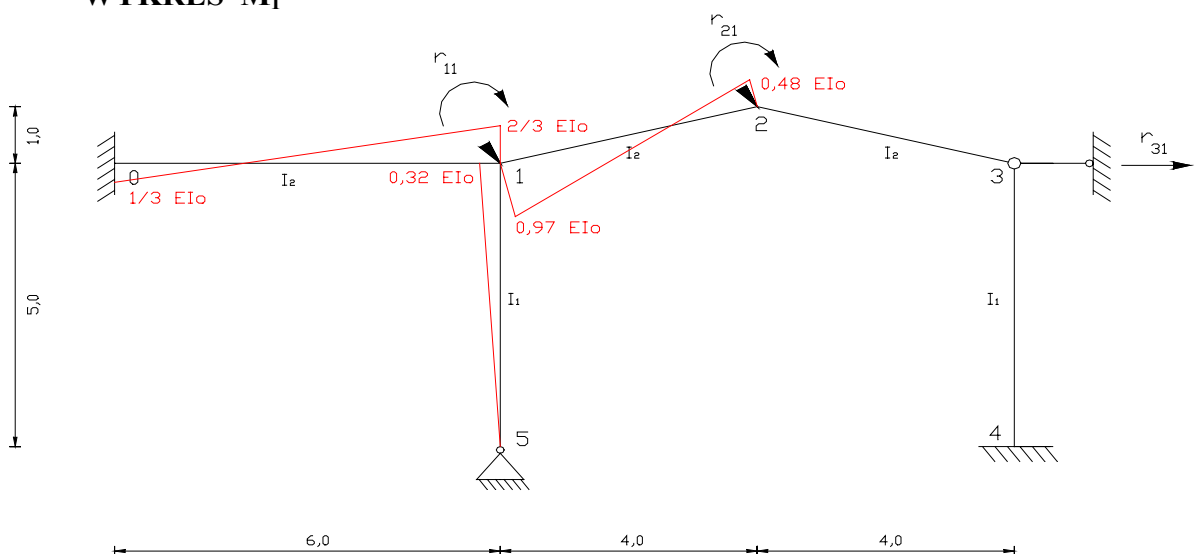
$$M_{23} = \frac{3EI_2}{l} \cdot (\varphi_2 - \psi_{23}) = \frac{3 \cdot EI_0}{\sqrt{17}} \cdot (0 - 0) = 0$$

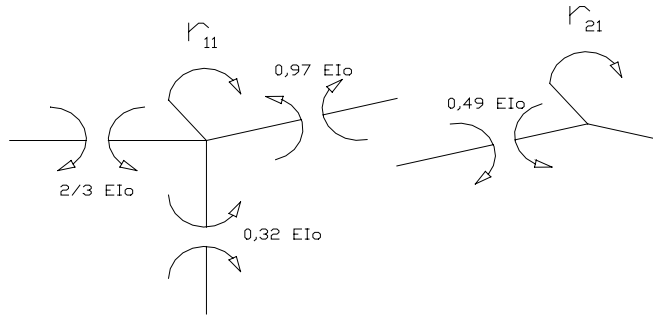
$$M_{32} = 0$$

$$M_{34} = 0$$

$$M_{43} = \frac{3EI_1}{l} \cdot (\varphi_4 - \psi_{34}) = \frac{3 \cdot 0,5331EI_0}{5} \cdot (0 - 0) = 0$$

WYKRES M_1





$$r_{11} = 0,97014EI_0 + 0,31986EI_0 + 2/3EI_0 = 1,95667EI_0$$

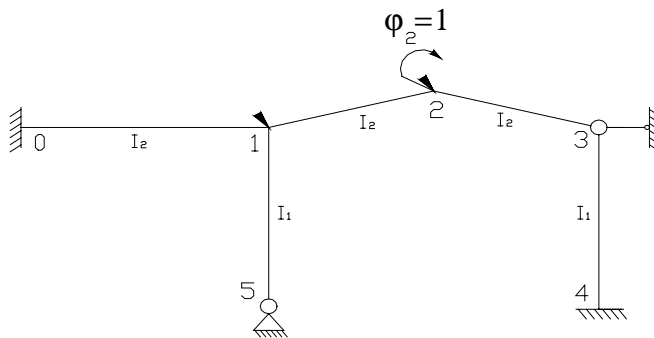
$$r_{21} = 0,48507EI_0$$

$$r_{31} \cdot \bar{1} + (1/3 + 2/3)EI_0 \cdot \psi_{01} + 0,31986EI_0 \cdot \psi_{15} + (0,97014 + 0,48507)EI_0 \cdot \psi_{12} = 0$$

$$r_{31} \cdot \bar{1} + (1/3 + 2/3)EI_0 \cdot 0 + 0,31986EI_0 \cdot 0 + (0,97014 + 0,48507)EI_0 \cdot \frac{1}{2} = 0$$

$$r_{31} = -0,727607EI_0$$

5. Stan $\varphi_2 = 1$.



$$M_{01} = \frac{2EI_2}{l} \cdot (2 \cdot \varphi_0 + \varphi_1 - 3 \cdot \psi_{01}) = \frac{2EI_0}{6} \cdot (2 \cdot 0 + 0 - 3 \cdot 0) = 0$$

$$M_{10} = \frac{2EI_2}{l} \cdot (2 \cdot \varphi_1 + \varphi_0 - 3 \cdot \psi_{01}) = \frac{2EI_0}{6} \cdot (2 \cdot 0 + 0 - 3 \cdot 0) = 0$$

$$M_{15} = \frac{3EI_1}{l} \cdot (\varphi_1 - \psi_{15}) = \frac{3 \cdot 0,5331EI_0}{5} \cdot (0 - 0) = 0$$

$$M_{51} = 0$$

$$M_{12} = \frac{2EI_2}{l} \cdot (2 \cdot \varphi_1 + \varphi_2 - 3 \cdot \psi_{12}) = \frac{2EI_0}{\sqrt{17}} \cdot (2 \cdot 0 + 1 - 3 \cdot 0) = 0,48507EI_0$$

$$M_{21} = \frac{2EI_2}{l} \cdot (2 \cdot \varphi_2 + \varphi_1 - 3 \cdot \psi_{12}) = \frac{2EI_0}{\sqrt{17}} \cdot (2 \cdot 1 + 0 - 3 \cdot 0) = 0,97014EI_0$$

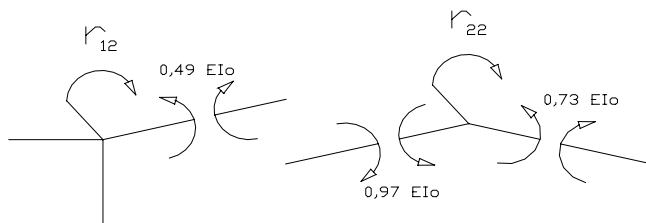
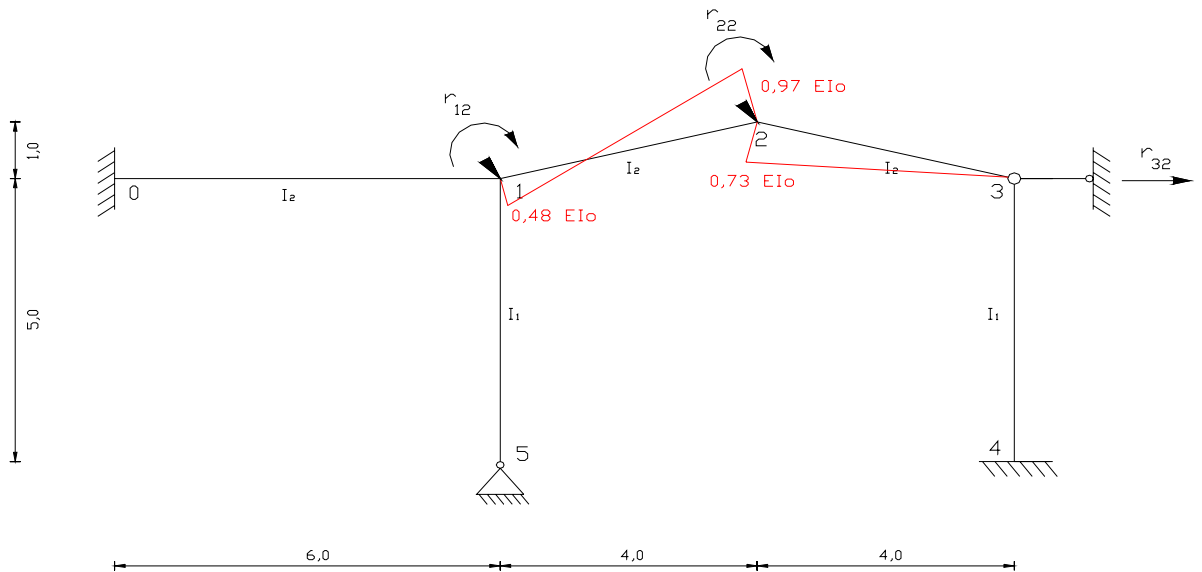
$$M_{23} = \frac{3EI_2}{l} \cdot (\varphi_2 - \psi_{23}) = \frac{3 \cdot EI_0}{\sqrt{17}} \cdot (1 - 0) = 0,727607EI_0$$

$$M_{32} = 0$$

$$M_{34} = 0$$

$$M_{43} = \frac{3EI_1}{l} \cdot (\varphi_4 - \psi_{34}) = \frac{3 \cdot 0,5331EI_0}{5} \cdot (0 - 0) = 0$$

WYKRES M_2



$$r_{12} = 0,48507EI_0$$

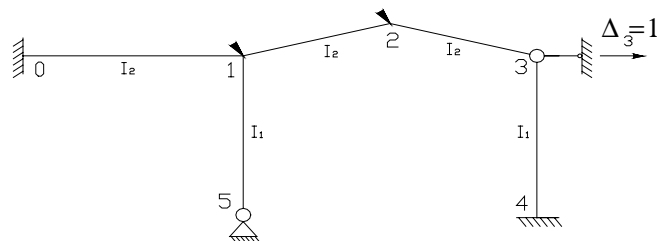
$$r_{22} = 0,727607EI_0 + 0,97014EI_0 = 1,697749EI_0$$

$$r_{32} \cdot 1 + (0,48507 + 0,97014)EI_0 \cdot \psi_{12} + 0,727607EI_0 \cdot \psi_{23} = 0$$

$$r_{32} \cdot 1 + (0,48507 + 0,97014)EI_0 \cdot \frac{1}{2} + 0,727607EI_0 \cdot \left(-\frac{1}{2}\right) = 0$$

$$r_{32} = -0,363803EI_0$$

6. Stan $\Delta_3 = 1$.



$$M_{01} = \frac{2EI_2}{l} \cdot (2 \cdot \varphi_0 + \varphi_1 - 3 \cdot \psi_{01}) = \frac{2EI_0}{6} \cdot (2 \cdot 0 + 0 - 3 \cdot 0) = 0$$

$$M_{10} = \frac{2EI_2}{l} \cdot (2 \cdot \varphi_1 + \varphi_0 - 3 \cdot \psi_{01}) = \frac{2EI_0}{6} \cdot (2 \cdot 0 + 0 - 3 \cdot 0) = 0$$

$$M_{15} = \frac{3EI_1}{l} \cdot (\varphi_1 - \psi_{15}) = \frac{3 \cdot 0,5331EI_0}{5} \cdot (0 - 0) = 0$$

$$M_{51} = 0$$

$$M_{12} = \frac{2EI_2}{l} \cdot (2 \cdot \varphi_1 + \varphi_2 - 3 \cdot \psi_{12}) = \frac{2EI_0}{\sqrt{17}} \cdot \left(2 \cdot 0 + 0 - 3 \cdot \frac{1}{2} \right) = -0,727607EI_0$$

$$M_{21} = \frac{2EI_2}{l} \cdot (2 \cdot \varphi_2 + \varphi_1 - 3 \cdot \psi_{12}) = \frac{2EI_0}{\sqrt{17}} \cdot \left(2 \cdot 0 + 0 - 3 \cdot \frac{1}{2} \right) = -0,727607EI_0$$

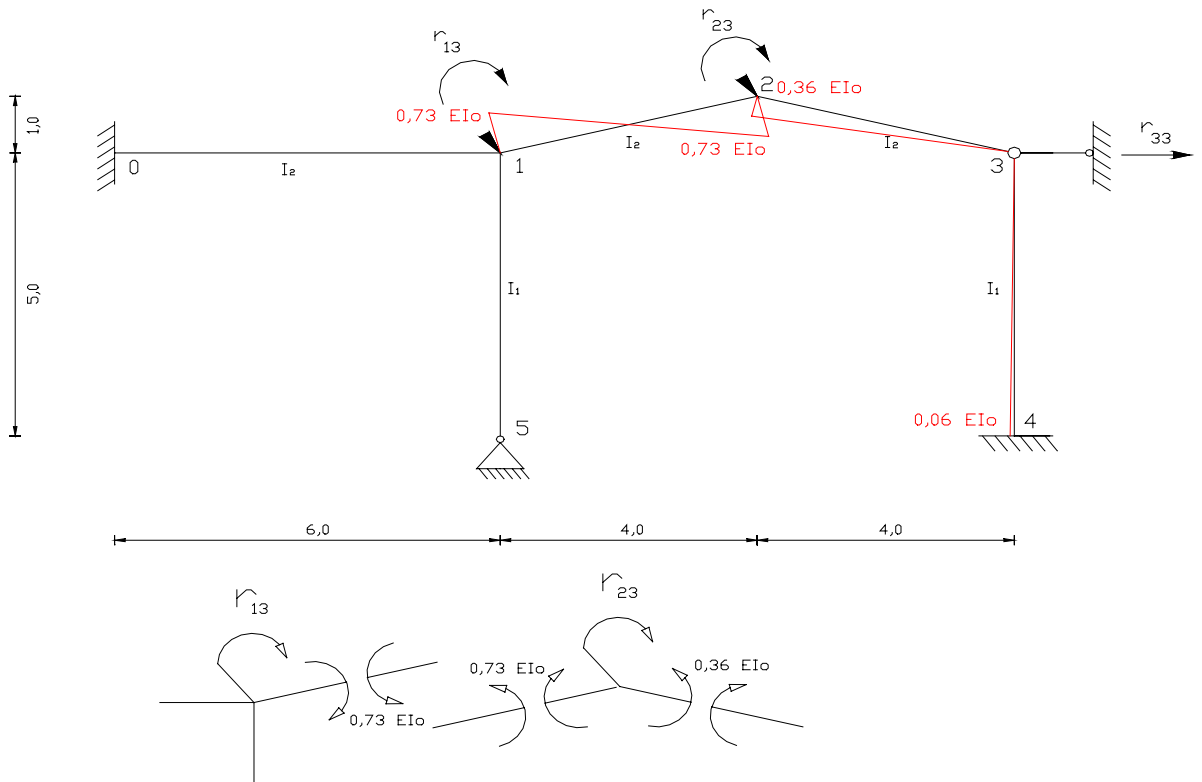
$$M_{23} = \frac{3EI_2}{l} \cdot (\varphi_2 - \psi_{23}) = \frac{3 \cdot EI_0}{\sqrt{17}} \cdot \left(0 + \frac{1}{2} \right) = 0,363803EI_0$$

$$M_{32} = 0$$

$$M_{34} = 0$$

$$M_{43} = \frac{3EI_1}{l} \cdot (\varphi_4 - \psi_{34}) = \frac{3 \cdot 0,5331EI_0}{5} \cdot \left(0 - \frac{1}{5} \right) = -0,063972EI_0$$

WYKRES M₃



$$r_{13} = -0,727607EI_0$$

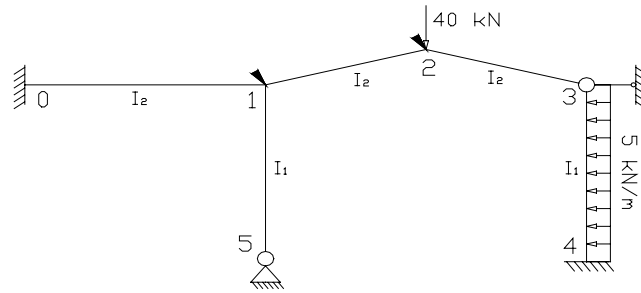
$$r_{23} = 0,363803EI_0 - 0,727607EI_0 = -0,363803$$

$$r_{33} \cdot \bar{1} + (-0,727607 - 0,727607)EI_0 \cdot \bar{\psi}_{12} + 0,363803EI_0 \cdot \bar{\psi}_{23} + (-0,063972)EI_0 \cdot \bar{\psi}_{34} = 0$$

$$r_{33} \cdot \bar{1} + (-0,727607 - 0,727607)EI_0 \cdot \frac{\bar{1}}{2} + 0,363803EI_0 \cdot \left(-\frac{\bar{1}}{2} \right) + (-0,063972)EI_0 \cdot \frac{\bar{1}}{5} = 0$$

$$r_{33} = 0,922303EI_0$$

7. Stan P.



$$M_{01} = M_{10} = 0 \text{ kNm}$$

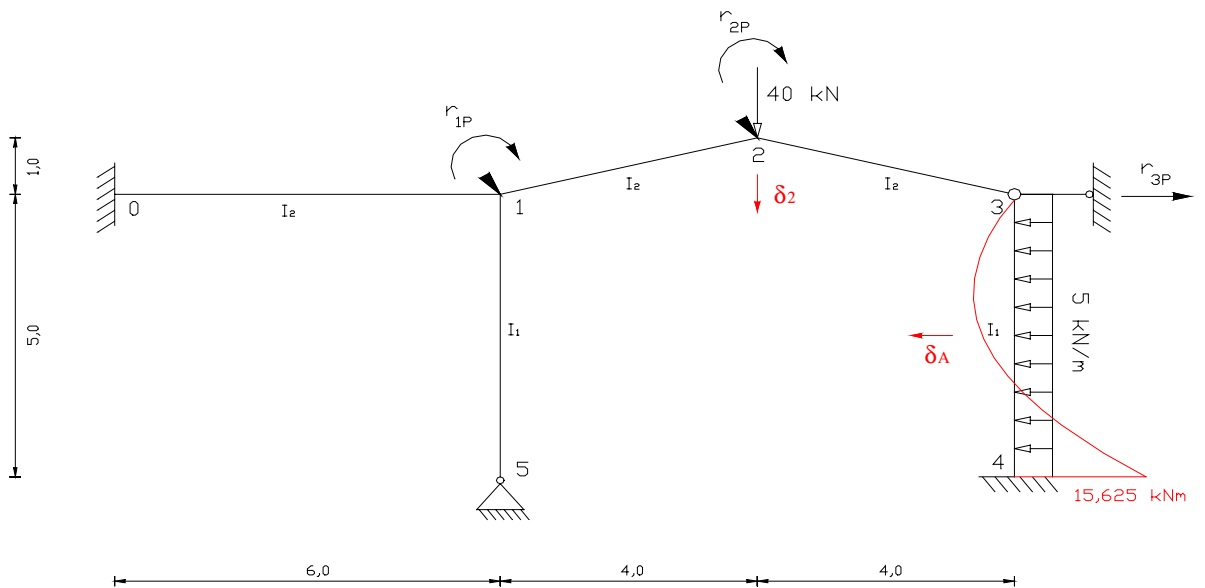
$$M_{12} = M_{21} = 0 \text{ kNm}$$

$$M_{23} = M_{32} = 0 \text{ kNm}$$

$$M_{34} = 0$$

$$M_{43} = \frac{q \cdot l^2}{8} = \frac{5 \cdot 5^2}{8} = 15,625 \text{ kNm}$$

WYKRES M_P^0



$$r_{1P} = 0 \text{ kNm}$$

$$r_{2P} = 0 \text{ kNm}$$

$$\uparrow 512 \quad 0 \cdot \Psi_{15} + 4 \cdot \Psi_{12} = -(-\delta_2) \rightarrow \delta_2 = 4\Delta/2 = 2\Delta$$

$$\rightarrow 4A \quad 2,5 \cdot \Psi_{34} = -\delta_A \rightarrow \delta_A = 2,5\Delta/5 = -0,5\Delta$$

$$r_{3P} \cdot \bar{1} - (-15,625) \cdot \bar{\psi}_{34} + 5 \cdot 5 \cdot \delta_A + 40 \cdot \delta_2 = 0$$

$$r_{3P} \cdot \bar{1} - (-15,625) \cdot \frac{\bar{1}}{5} - 5 \cdot 5 \cdot 0,5 \cdot \bar{1} + 40 \cdot 2 \cdot \bar{1} = 0$$

$$r_{3P} = -70,625 \text{ kNm}$$

8. Rozwiązanie układu równań kanonicznych.

$$r_{11} \cdot \varphi_1 + r_{12} \cdot \varphi_2 + r_{13} \cdot \Delta_3 + r_{1P} = 0$$

$$r_{21} \cdot \varphi_1 + r_{22} \cdot \varphi_2 + r_{23} \cdot \Delta_3 + r_{2P} = 0$$

$$r_{31} \cdot \varphi_1 + r_{32} \cdot \varphi_2 + r_{33} \cdot \Delta_3 + r_{3P} = 0$$

$$1,95667 EI_0 \cdot \varphi_1 + 0,48507 EI_0 \cdot \varphi_2 - 0,72760 EI_0 \cdot \Delta_3 + 0 = 0$$

$$0,48507 EI_0 \cdot \varphi_1 + 1,69774 EI_0 \cdot \varphi_2 - 0,36380 EI_0 \cdot \Delta_3 + 0 = 0$$

$$-0,72760 EI_0 \cdot \varphi_1 - 0,36380 EI_0 \cdot \varphi_2 + 0,92230 EI_0 \cdot \Delta_3 - 70,625 = 0$$

Obliczenia przeprowadzono w arkuszu kalkulacyjnym Microsoft Excel poprzez odwrócenie macierzy.

$$\varphi_1 = \frac{38,430476}{EI_0}$$

$$\varphi_2 = \frac{13,026492}{EI_0}$$

$$\Delta_3 = \frac{112,030817}{EI_0}$$

9. Wyznaczenie wartości momentów zginających.

Stosując zasadę superpozycji otrzymamy:

$$M_P^n = M_1 \cdot \varphi_1 + M_2 \cdot \varphi_2 + M_3 \cdot \Delta_3 + M_P^0 \text{ [kNm]}$$

$$M_{01} = \frac{1}{3} EI_0 \cdot \frac{38,430}{EI_0} + 0 \cdot \frac{13,026}{EI_0} + 0 \cdot \frac{112,031}{EI_0} + 0 = 12,810 \text{ kNm}$$

$$M_{10} = \frac{2}{3} EI_0 \cdot \frac{38,430}{EI_0} + 0 \cdot \frac{13,026}{EI_0} + 0 \cdot \frac{112,031}{EI_0} + 0 = 25,620 \text{ kNm}$$

$$M_{15} = 0,320 EI_0 \cdot \frac{38,430}{EI_0} + 0 \cdot \frac{13,026}{EI_0} + 0 \cdot \frac{112,031}{EI_0} + 0 = 12,292 \text{ kNm}$$

$$M_{51} = \frac{38,430}{EI_0} + 0 \cdot \frac{13,026}{EI_0} + 0 \cdot \frac{112,031}{EI_0} + 0 = 0 \text{ kNm}$$

$$M_{12} = 0,970 EI_0 \cdot \frac{38,430}{EI_0} + 0,485 EI_0 \cdot \frac{13,026}{EI_0} - 0,728 EI_0 \cdot \frac{112,031}{EI_0} + 0 = -37,913 \text{ kNm}$$

$$M_{21} = 0,485 EI_0 \cdot \frac{38,430}{EI_0} + 0,970 EI_0 \cdot \frac{13,026}{EI_0} - 0,728 EI_0 \cdot \frac{112,031}{EI_0} + 0 = -50,235 \text{ kNm}$$

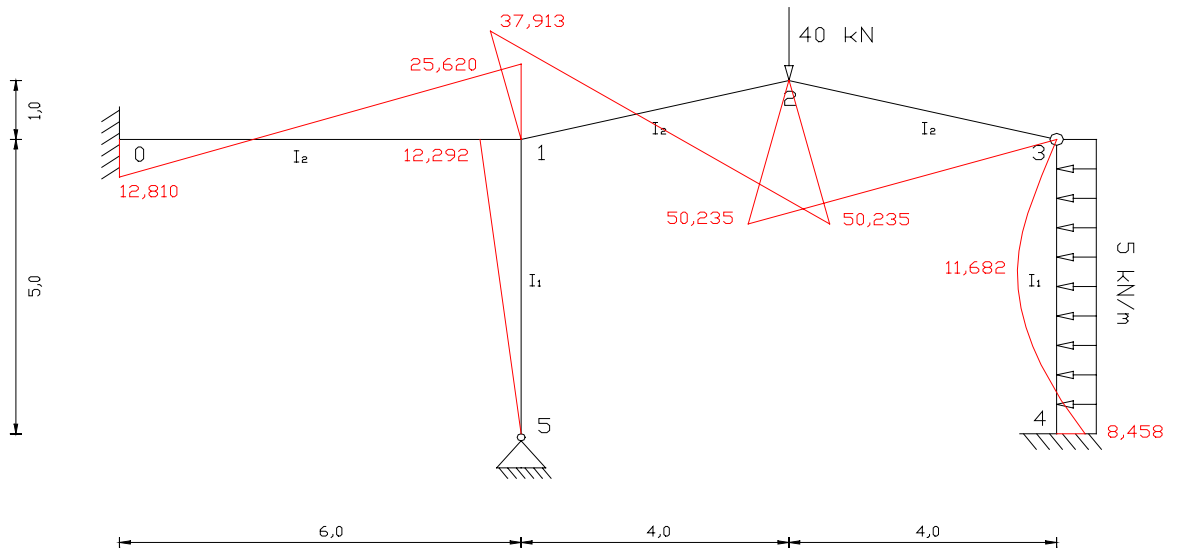
$$M_{23} = 0 \cdot \frac{38,430}{EI_0} + 0,728 EI_0 \cdot \frac{13,026}{EI_0} + 0,364 EI_0 \cdot \frac{112,031}{EI_0} + 0 = 50,235 \text{ kNm}$$

$$M_{32} = 0 \text{ kNm}$$

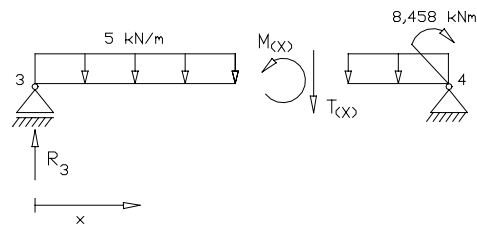
$$M_{34} = 0 \text{ kNm}$$

$$M_{43} = 0 \cdot \frac{38,430}{EI_0} + 0 \cdot \frac{13,026}{EI_0} - 0,064EI_0 \cdot \frac{112,031}{EI_0} + 15,625 = 8,458 \text{ kNm}$$

WYKRES M_P^n [kNm]



Wyznaczenie M_{\max}



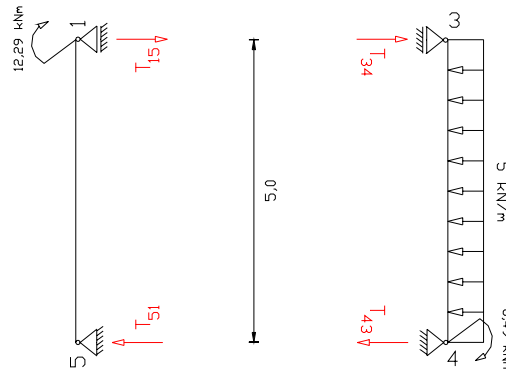
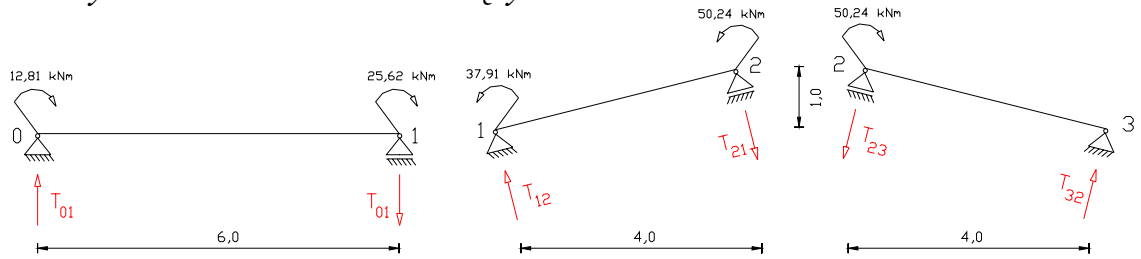
$$\begin{aligned} \sum M_4 = 0 \\ R_3 \cdot 5 - 5 \cdot 5 \cdot 2,5 + 8,458 = 0 \\ R_3 = 10,808 \text{ kN} \end{aligned}$$

$$\begin{aligned} T(x) &= -5x + R_3 = -5x + 10,808 \\ M(x) &= R_3 \cdot x - 5 \cdot x \cdot x/2 = -5/2x^2 + 10,808x \end{aligned}$$

$$\begin{aligned} T_{(x_0)} &= 0 \\ -5x_0 + 10,808 &= 0 \\ x_0 &= 2,16 \text{ m} \end{aligned}$$

$$\begin{aligned} M_{\max} &= M_{(x_0)} = -5/2 \cdot 2,16^2 + 10,808 \cdot 2,16 \\ M_{\max} &= 11,682 \text{ kNm} \end{aligned}$$

10. Wyznaczenie wartości sił tnących.



$$T_{01} = T_{10} = -\frac{12,81 + 25,62}{6} = -6,405 \text{ kN}$$

$$T_{12} = T_{21} = \frac{37,91 + 50,24}{\sqrt{17}} = 21,379 \text{ kN}$$

$$T_{23} = T_{32} = -\frac{50,24}{\sqrt{17}} = -12,184 \text{ kN}$$

$$T_{15} = T_{51} = -\frac{12,29}{5} = -2,458 \text{ kN}$$

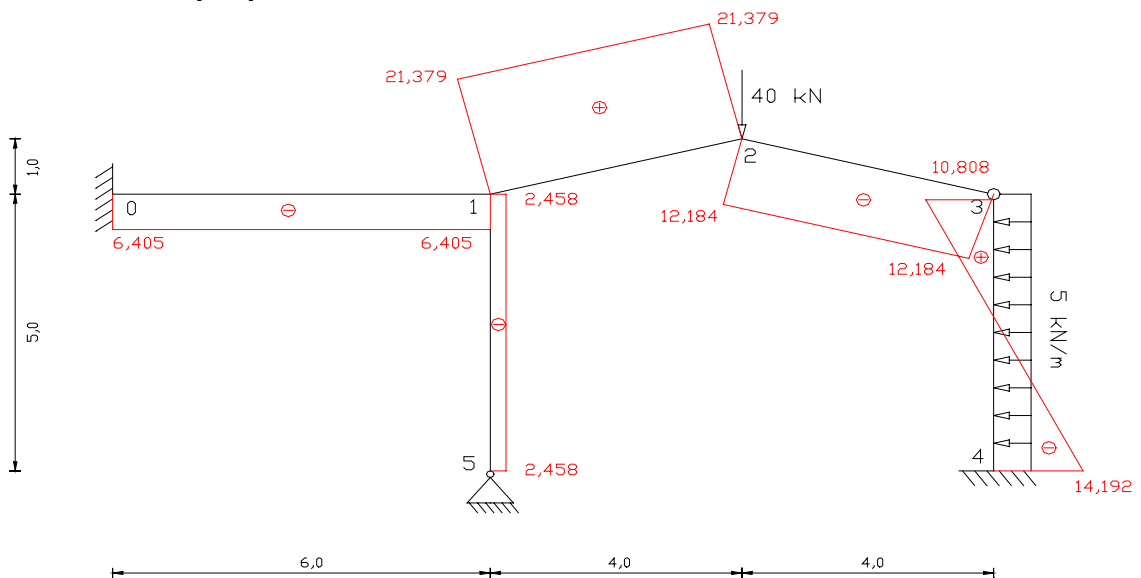
$$\sum M_4 = 0 \quad T_{34} \cdot 5 - 5 \cdot 5 \cdot 2,5 + 8,46 = 0$$

$$\rightarrow T_{34} = 10,808 \text{ kN}$$

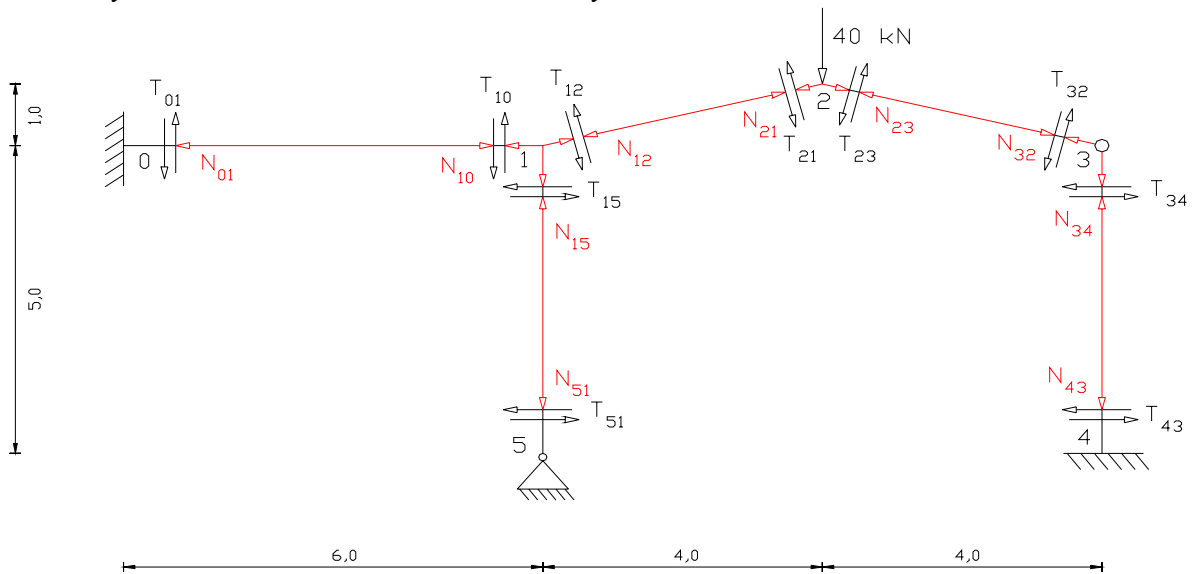
$$\sum M_3 = 0 \quad T_{43} \cdot 5 + 5 \cdot 5 \cdot 2,5 + 8,46 = 0$$

$$\rightarrow T_{43} = -14,192 \text{ kN}$$

WYKRES T [kN]



11. Wyznaczenie wartości sił normalnych.



$$\sin\alpha = 0,242536; \quad \cos\alpha = 0,970732$$

WEZEL 3

$$\sum X = 0 \quad -N_{32} \cdot \cos\alpha + T_{32} \cdot \sin\alpha - T_{34} = 0$$

$$N_{32} = -14,178 \text{ kN}$$

$$\sum Y = 0 \quad -N_{34} + N_{32} \cdot \sin\alpha - T_{32} \cdot \cos\alpha = 0$$

$$N_{34} = -15,266 \text{ kN}$$

PRĘT 2-3

$$\sum X = 0 \quad N_{32} = N_{23} = -14,178 \text{ kN (ponieważ } T_{32} = T_{23})$$

PRĘT 3-4

$$\sum Y = 0 \quad N_{43} = N_{34} = -15,266 \text{ kN}$$

WEZEL 2

$$\sum X = 0 \quad -N_{21} \cdot \cos\alpha - T_{21} \cdot \sin\alpha + N_{23} \cdot \cos\alpha - T_{23} \cdot \sin\alpha = 0$$

$$N_{21} = -16,476 \text{ kN}$$

PRĘT 1-2

$$\sum X = 0 \quad N_{12} = N_{21} = -16,476 \text{ kN (ponieważ } T_{12} = T_{21})$$

WEZEL 1

$$\sum X = 0 \quad -N_{10} + N_{12} \cdot \cos\alpha + T_{12} \cdot \sin\alpha - T_{15} = 0$$

$$N_{10} = -8,350 \text{ kN}$$

$$\sum Y = 0 \quad -N_{15} + N_{12} \cdot \sin\alpha - T_{12} \cdot \cos\alpha + T_{10} = 0$$

$$N_{15} = -31,154 \text{ kN}$$

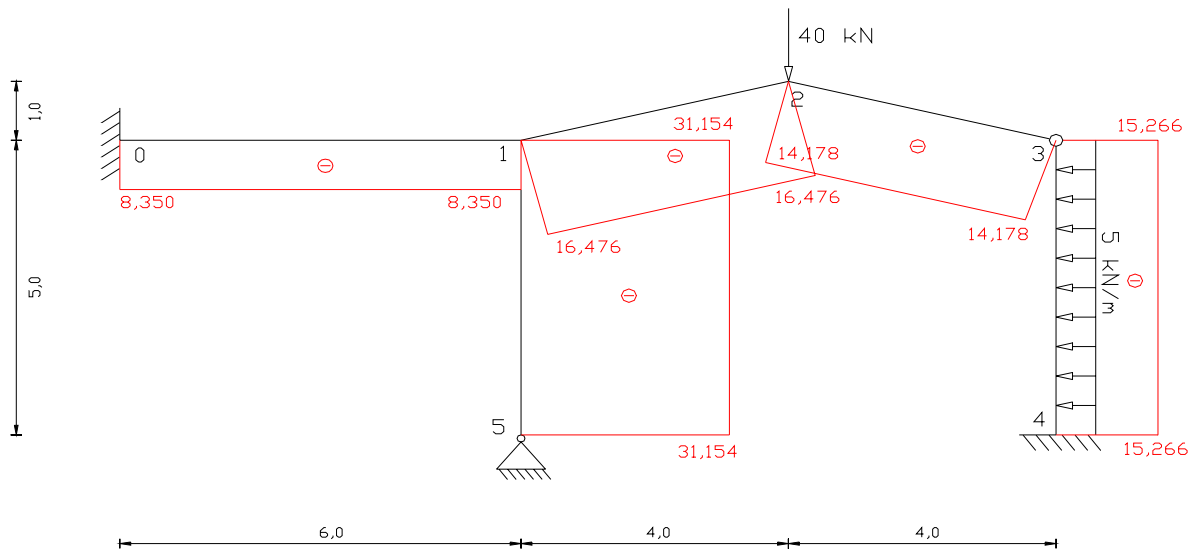
PRĘT 0-1

$$\sum X = 0 \quad N_{01} = N_{10} = -8,350 \text{ kN}$$

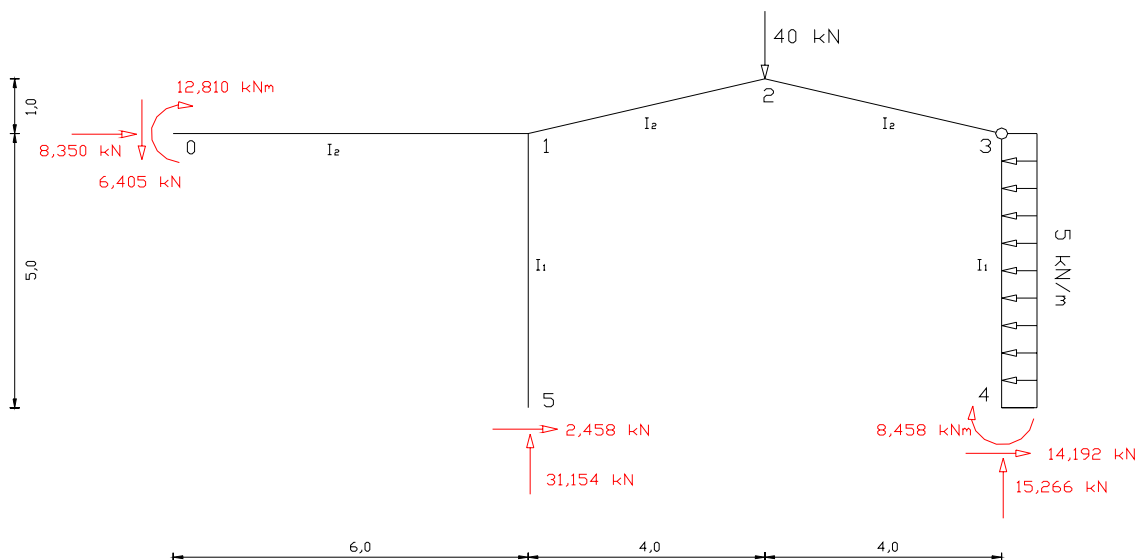
PRĘT 1-5

$$\sum Y = 0 \quad N_{15} = N_{51} = -31,154 \text{ kN}$$

WYKRES N [kN]



12. Kontrola statyczna.



$$\begin{aligned} \sum M_4 = 0 \\ 8,350 \cdot 5 - 6,405 \cdot 14 + 12,810 + 31,154 \cdot 8 - 40 \cdot 4 - 5 \cdot 5 \cdot 2,5 + 8,458 = 0 \\ 0,0812 \approx 0 \end{aligned}$$

$$\begin{aligned} \sum X = 0 \\ 8,350 + 2,458 + 14,192 - 5 \cdot 5 = 0 \\ 0 = 0 \end{aligned}$$

$$\begin{aligned} \sum Y = 0 \\ -6,405 + 31,154 - 40 + 15,266 = 0 \\ 0,0153 \approx 0 \end{aligned}$$