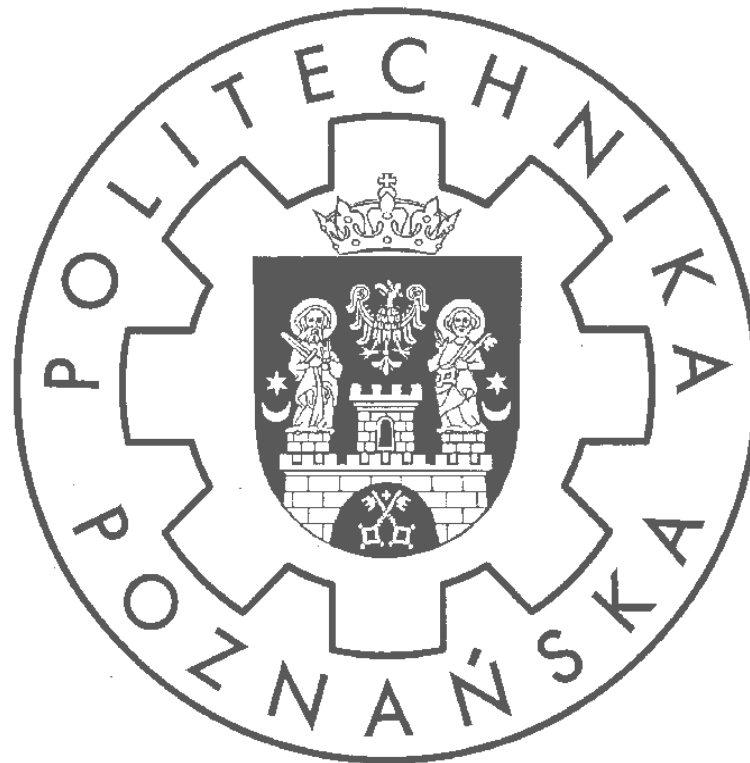


Politechnika Poznańska
Instytut Konstrukcji Budowlanych
Zakład Mechaniki Budowli



Ćwiczenie projektowe nr 2

Dynamika – ujęcie klasyczne

Prowadzący:

Autor:

Nr indeksu:

Semestr:

Rok:

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Robert Dybionka

Jakub Stasiak

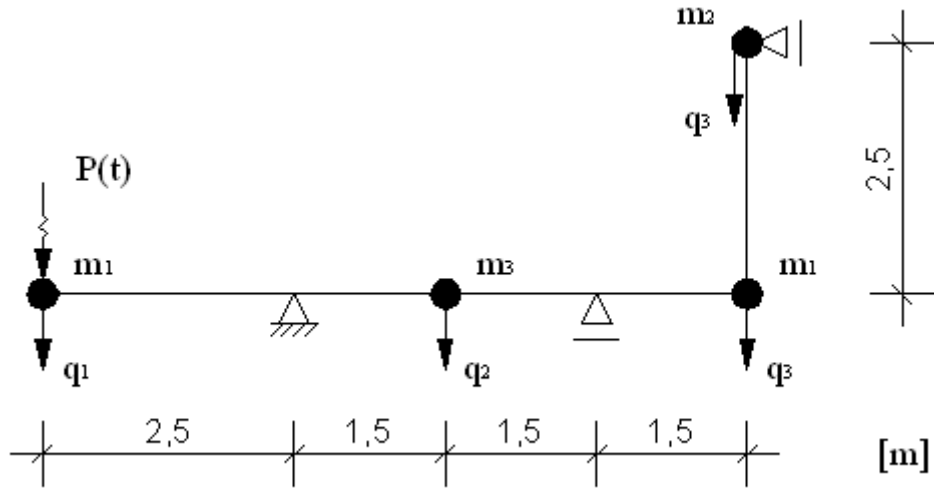
113012, 113010

IV (pierwszy stopień)

2013/2014

Ćwiczenie projektowe nr 2 – Dynamika – ujęcie klasyczne

1. Schemat statyczny i stopień dynamicznej swobody konstrukcji:



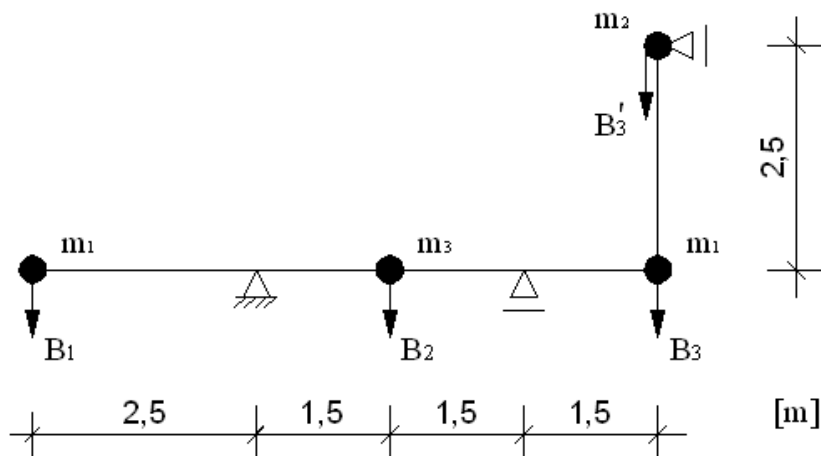
SSD = 3

2. Dane wyjściowe do projektu:

- $E = 205 \text{ GPa}$
- I200 IPE - $I = 1940 \text{ cm}^4$
- $EI = 3977 \text{ kNm}^2 = 3977000 \text{ Nm}^2$
- $m_1 = 320 \text{ kg}$
- $m_2 = 430 \text{ kg}$
- $m_3 = 540 \text{ kg}$
- $P = P_0 = 62,3 \text{ kN} = 62300 \text{ N}$
- $p = 28,0 \text{ Hz} = 175,9292 \frac{\text{rad}}{\text{s}}$

I. DRGANIA WŁASNE:

1. Siły działające na układ:



$$q_1 = A_1 \cdot \sin(\omega t)$$

$$q_2 = A_2 \cdot \sin(\omega t)$$

$$q_3 = A_3 \cdot \sin(\omega t)$$

$$\ddot{q}_1 = -A_1 \cdot \omega^2 \cdot \sin(\omega t)$$

$$\ddot{q}_2 = -A_2 \cdot \omega^2 \cdot \sin(\omega t)$$

$$\ddot{q}_3 = -A_3 \cdot \omega^2 \cdot \sin(\omega t)$$

$$B_1 = -m_1 \cdot \ddot{q}_1$$

$$B_2 = -m_3 \cdot \ddot{q}_2$$

$$B_3 = -m_1 \cdot \ddot{q}_3$$

$$B'_3 = -m_2 \cdot \ddot{q}_3$$

$$\begin{cases} q_1 = \delta_{11} \cdot B_1 + \delta_{12} \cdot B_2 + \delta_{13} \cdot (B_3 + B'_3) \\ q_2 = \delta_{21} \cdot B_1 + \delta_{22} \cdot B_2 + \delta_{23} \cdot (B_3 + B'_3) \\ q_3 = \delta_{31} \cdot B_1 + \delta_{32} \cdot B_2 + \delta_{33} \cdot (B_3 + B'_3) \end{cases}$$

$$\begin{cases} A_1 \sin(\omega t) = \delta_{11} \cdot 320,0 \cdot A_1 \cdot \omega^2 \sin(\omega t) + \delta_{12} \cdot 540,0 \cdot A_2 \cdot \omega^2 \sin(\omega t) + \delta_{13} \cdot (320,0 + 430,0) \cdot A_3 \cdot \omega^2 \sin(\omega t) \\ A_2 \sin(\omega t) = \delta_{21} \cdot 320,0 \cdot A_1 \cdot \omega^2 \sin(\omega t) + \delta_{22} \cdot 540,0 \cdot A_2 \cdot \omega^2 \sin(\omega t) + \delta_{23} \cdot (320,0 + 430,0) \cdot A_3 \cdot \omega^2 \sin(\omega t) \\ A_3 \sin(\omega t) = \delta_{31} \cdot 320,0 \cdot A_1 \cdot \omega^2 \sin(\omega t) + \delta_{32} \cdot 540,0 \cdot A_2 \cdot \omega^2 \sin(\omega t) + \delta_{33} \cdot (320,0 + 430,0) \cdot A_3 \cdot \omega^2 \sin(\omega t) \end{cases}$$

$$\begin{cases} A_1 = \delta_{11} \cdot 320,0 \cdot A_1 \cdot \omega^2 + \delta_{12} \cdot 540,0 \cdot A_2 \cdot \omega^2 + \delta_{13} \cdot (320,0 + 430,0) \cdot A_3 \cdot \omega^2 \\ A_2 = \delta_{21} \cdot 320,0 \cdot A_1 \cdot \omega^2 + \delta_{22} \cdot 540,0 \cdot A_2 \cdot \omega^2 + \delta_{23} \cdot (320,0 + 430,0) \cdot A_3 \cdot \omega^2 \\ A_3 = \delta_{31} \cdot 320,0 \cdot A_1 \cdot \omega^2 + \delta_{32} \cdot 540,0 \cdot A_2 \cdot \omega^2 + \delta_{33} \cdot (320,0 + 430,0) \cdot A_3 \cdot \omega^2 \end{cases}$$

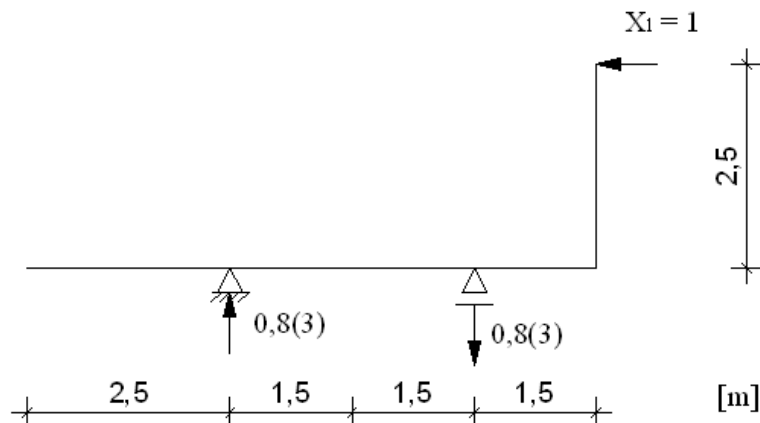
$$\begin{cases} A_1(1 - \delta_{11} \cdot 320,0 \cdot \omega^2) - \delta_{12} \cdot 540,0 \cdot A_2 \cdot \omega^2 - \delta_{13} \cdot (320,0 + 430,0) \cdot A_3 \cdot \omega^2 = 0 \\ -\delta_{21} \cdot 320,0 \cdot A_1 \cdot \omega^2 + A_2(1 - \delta_{22} \cdot 540,0 \cdot \omega^2) + \delta_{23} \cdot (320,0 + 430,0) \cdot A_3 \cdot \omega^2 = 0 \\ -\delta_{31} \cdot 320,0 \cdot A_1 \cdot \omega^2 - \delta_{32} \cdot 540,0 \cdot A_2 \cdot \omega^2 + A_3(1 - \delta_{33} \cdot (320,0 + 430,0) \cdot \omega^2) = 0 \end{cases}$$

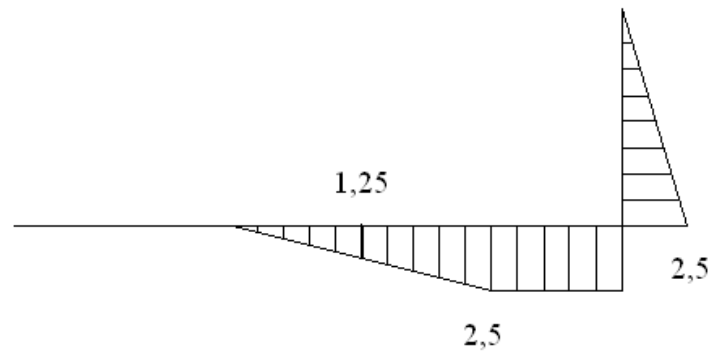
2. Obliczenie współczynników δ_{ik} :

$$\delta_{ik} = \sum \int \frac{M_i \cdot M_k}{EI} dx, \quad M_i, M_k - \text{momenty zginające wywołane jednostkową siłą po kierunku odpowiednio } q_i \text{ oraz } q_k$$

➤ Wyznaczenie M_1^n :

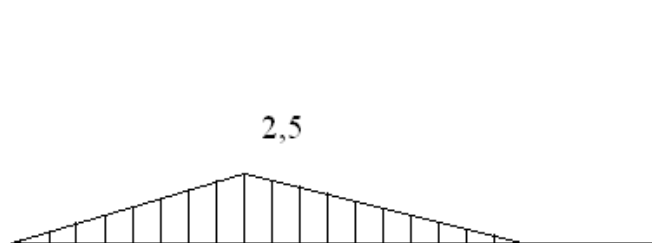
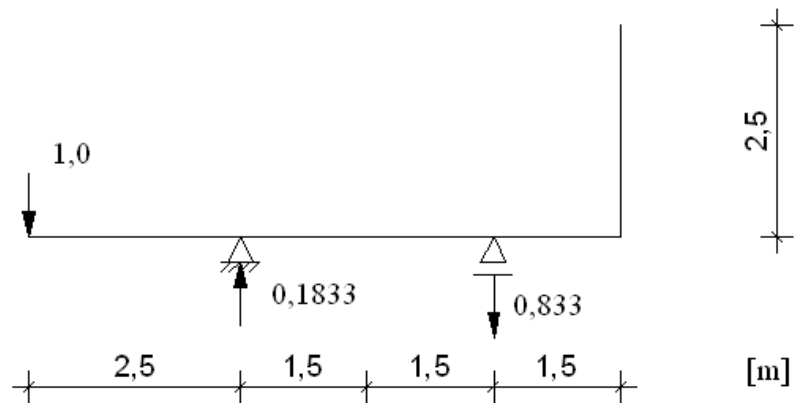
- Stan $X_1 = 1$:





M_1

- Stan „P₁” - siła jednostkowa po kierunku q₁:



M_p^0

$$\delta_{11} = \frac{1}{EI} \left[\frac{1}{2} \cdot 2,5 \cdot 2,5 \cdot \frac{2}{3} \cdot 2,5 + \frac{1}{2} \cdot 3,0 \cdot 2,5 \cdot \frac{2}{3} \cdot 2,5 + 2,5 \cdot 1,5 \cdot 2,5 \right]$$

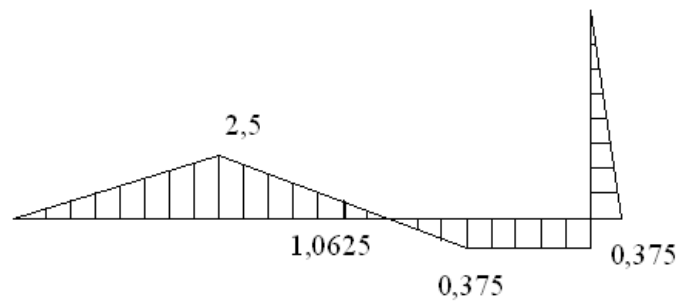
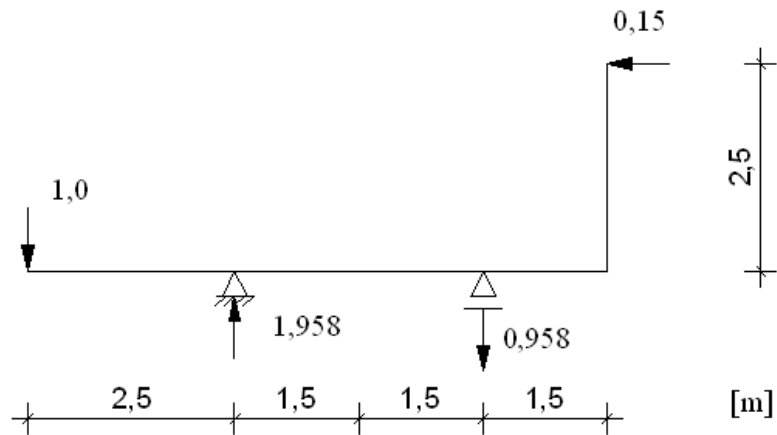
$$\delta_{11} = \frac{20,8333}{EI}$$

$$\delta_{1P} = \frac{1}{EI} \left[-\frac{1}{2} \cdot 2,5 \cdot 3,0 \cdot \frac{1}{3} \cdot 2,5 \right]$$

$$\delta_{1P} = -\frac{3,125}{EI}$$

$$X_1 = -\frac{\delta_{1P}}{\delta_{11}}$$

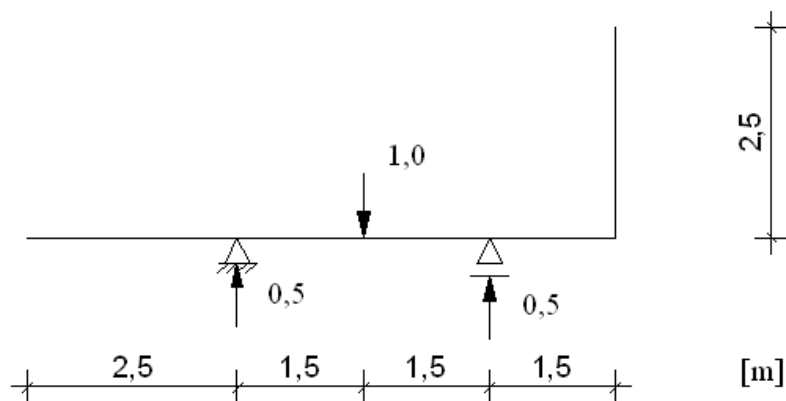
$$X_1 = 0,15$$

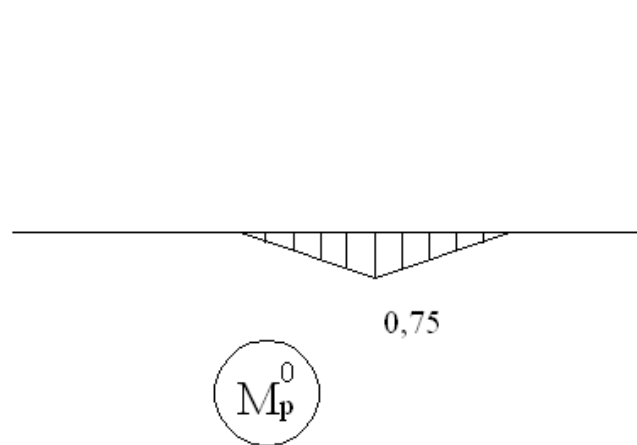


M_i^n

➤ Wyznaczenie M_2^n :

- Stan $X_1 = 1$ – jak poprzednio (str. 3):
- Stan „P” - siła jednostkowa po kierunku q_2 :





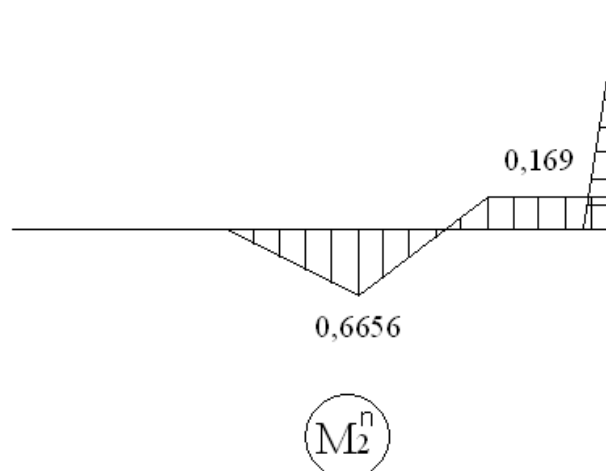
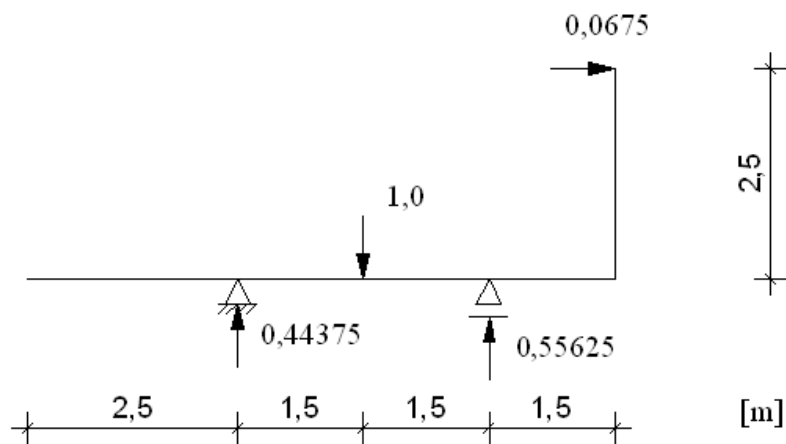
$$\delta_{11} = \frac{20,8333}{EI}$$

$$\delta_{1P} = \frac{1}{EI} \left[\frac{1}{2} \cdot 1,5 \cdot 0,75 \cdot \frac{2}{3} \cdot 1,25 + \frac{1}{2} \cdot 1,5 \cdot 0,75 \cdot \left(\frac{2}{3} \cdot 1,25 + \frac{1}{3} \cdot 2,5 \right) \right]$$

$$\delta_{1P} = \frac{1,40625}{EI}$$

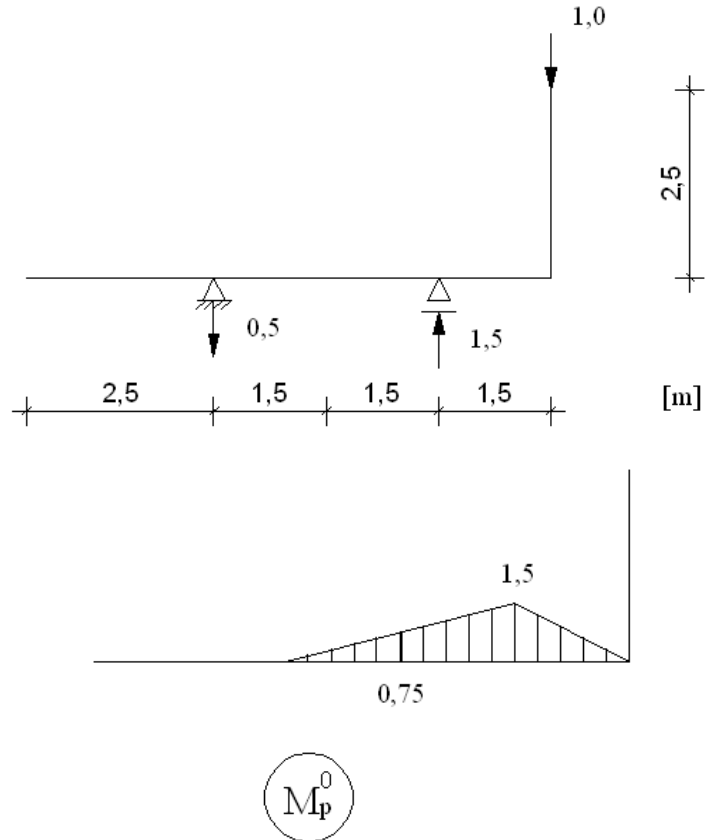
$$X_1 = - \frac{\delta_{1P}}{\delta_{11}}$$

$$X_1 = - 0,0675$$



➤ Wyznaczenie M_3^n :

- Stan $X_1 = 1$ – jak poprzednio (str. 3):
- Stan „P” - siła jednostkowa po kierunku q_3 :

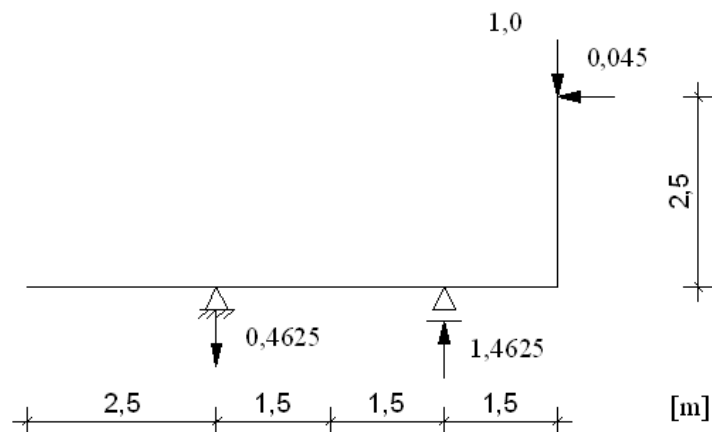


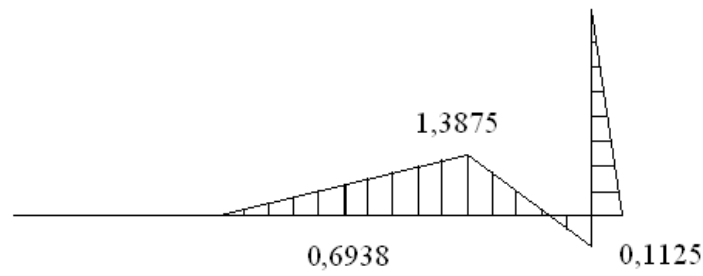
$$\delta_{11} = \frac{20,8333}{EI}$$

$$\delta_{1P} = \frac{1}{EI} \left[-\frac{1}{2} \cdot 1,5 \cdot 3,0 \cdot \frac{2}{3} \cdot 2,5 - \frac{1}{2} \cdot 1,5 \cdot 1,5 \cdot 2,5 \right] = -\frac{0,9375}{EI}$$

$$X_1 = -\frac{\delta_{1P}}{\delta_{11}}$$

$$X_1 = 0,045$$





$$\textcircled{MB^n}$$

$$\delta_{ik} = \sum \int \frac{M_i^n \cdot M_k^n}{EI} dx$$

$$\delta_{11} = \frac{1}{EI} \left[\frac{1}{2} \cdot 2,5 \cdot 2,5 \cdot \frac{2}{3} \cdot 2,5 + \frac{1}{2} \cdot 2,5 \cdot 3,0 \cdot \left(\frac{2}{3} \cdot 2,5 - \frac{1}{3} \cdot 0,375 \right) + \frac{1}{2} \cdot 0,375 \cdot 3,0 \cdot \left(\frac{2}{3} \cdot 0,375 - \frac{1}{3} \cdot 2,5 \right) + 0,375 \cdot 1,5 \cdot 0,375 + \frac{1}{2} \cdot 0,375 \cdot 2,5 \cdot \frac{2}{3} \cdot 0,375 \right]$$

$$\delta_{11} = \frac{10,99}{EI}$$

$$\delta_{22} = \frac{1}{EI} \left[\frac{1}{2} \cdot 1,5 \cdot 0,6656 \cdot \frac{2}{3} \cdot 0,6656 + \frac{1}{2} \cdot 0,6656 \cdot 1,5 \cdot \left(\frac{2}{3} \cdot 0,6656 - \frac{1}{3} \cdot 0,169 \right) + \frac{1}{2} \cdot 1,5 \cdot 0,169 \cdot \left(\frac{2}{3} \cdot 0,169 - \frac{1}{3} \cdot 0,6656 \right) + 0,169 \cdot 1,5 \cdot 0,169 + \frac{1}{2} \cdot 2,5 \cdot 0,169 \cdot \frac{2}{3} \cdot 0,169 \right]$$

$$\delta_{22} = \frac{0,4677}{EI}$$

$$\delta_{33} = \frac{1}{EI} \left[\frac{1}{2} \cdot 1,3875 \cdot 3,0 \cdot \frac{2}{3} \cdot 1,3875 + \frac{1}{2} \cdot 1,3875 \cdot 1,5 \cdot \left(\frac{2}{3} \cdot 1,3875 - \frac{1}{3} \cdot 0,1125 \right) + \frac{1}{2} \cdot 0,1125 \cdot 1,5 \cdot \left(\frac{2}{3} \cdot 0,1125 - \frac{1}{3} \cdot 1,3875 \right) + \frac{1}{2} \cdot 0,1125 \cdot 2,5 \cdot \frac{2}{3} \cdot 0,1125 \right]$$

$$\delta_{33} = \frac{2,8266}{EI}$$

$$\delta_{12} = \frac{1}{EI} \left[-\frac{1}{2} \cdot 1,5 \cdot 0,6656 \cdot \left(\frac{2}{3} \cdot 1,0625 + \frac{1}{3} \cdot 2,5 \right) + \frac{1}{2} \cdot 0,6656 \cdot 1,5 \cdot \left(-\frac{2}{3} \cdot 1,0625 + \frac{1}{3} \cdot 0,375 \right) + \frac{1}{2} \cdot 1,5 \cdot 0,169 \cdot \left(-\frac{2}{3} \cdot 0,375 + \frac{1}{3} \cdot 1,0625 \right) - 0,169 \cdot 1,5 \cdot 0,375 - \frac{1}{2} \cdot 2,5 \cdot 0,169 \cdot \frac{2}{3} \cdot 0,375 \right]$$

$$\delta_{12} = -\frac{1,0}{EI}$$

$$\delta_{13} = \frac{1}{EI} \left[\frac{1}{2} \cdot 1,3875 \cdot 3,0 \cdot \left(-\frac{2}{3} \cdot 0,375 + \frac{1}{3} \cdot 2,5 \right) - \frac{1}{2} \cdot 1,5 \cdot 1,3875 \cdot 0,375 + \frac{1}{2} \cdot 0,1125 \cdot 1,5 \cdot 0,375 + \frac{1}{2} \cdot 0,1125 \cdot 2,5 \cdot \frac{2}{3} \cdot 0,375 \right]$$

$$\delta_{13} = \frac{0,8906}{EI}$$

$$\delta_{23} = \frac{1}{EI} \left[-\frac{1}{2} \cdot 0,6656 \cdot 1,5 \cdot \frac{2}{3} \cdot 0,69 - \frac{1}{2} \cdot 1,5 \cdot 0,6656 \cdot \left(\frac{2}{3} \cdot 0,69 + \frac{1}{3} \cdot 1,3875 \right) + \right]$$

$$\delta_{23} = -\frac{0,3984}{EI}$$

$$\begin{cases} A_1 \left(1 - \frac{10,99}{EI} \cdot 320,0 \cdot \omega^2\right) + \frac{1,0}{EI} \cdot 540,0 \cdot A_2 \cdot \omega^2 - \frac{0,8906}{EI} \cdot (320,0 + 430,0) \cdot A_3 \cdot \omega^2 = 0 \\ \frac{1,0}{EI} \cdot 320,0 \cdot A_1 \cdot \omega^2 + A_2 \left(1 - \frac{0,4677}{EI} \cdot 540,0 \cdot \omega^2\right) + \frac{0,3984}{EI} \cdot (320,0 + 430,0) \cdot A_3 \cdot \omega^2 = 0 \\ -\frac{0,8906}{EI} \cdot 320,0 \cdot A_1 \cdot \omega^2 + \frac{0,3984}{EI} \cdot 540,0 \cdot A_2 \cdot \omega^2 + A_3 \left(1 - \frac{2,8266}{EI} \cdot (320,0 + 430,0)\right) \cdot \omega^2 = 0 \end{cases}$$

$$\lambda = \frac{\omega^2}{EI}$$

$$\begin{cases} A_1(1 - 3516,8 \cdot \lambda) + 540,0 \cdot A_2 \cdot \lambda - 667,5 \cdot A_3 \cdot \lambda = 0 \\ 320,0 \cdot A_1 \cdot \lambda + A_2(1 - 252,558 \cdot \lambda) + 298,5 \cdot A_3 \cdot \lambda = 0 \\ -284,8 \cdot A_1 \cdot \lambda + 214,92 \cdot A_2 \cdot \lambda + A_3(1 - 2119,95 \cdot \lambda) = 0 \end{cases}$$

- Wyznacznik:

$$\begin{vmatrix} (1 - 3516,8 \cdot \lambda) & 540,0 \cdot \lambda & -667,5 \cdot \lambda \\ 320,0 \cdot \lambda & (1 - 252,558 \cdot \lambda) & 298,5 \cdot \lambda \\ -284,8 \cdot \lambda & 214,92 \cdot \lambda & (1 - 2119,95 \cdot \lambda) \end{vmatrix} = 0$$

- Wartości obliczonych współczynników λ :

$$\lambda_1 = 0,0002699$$

$$\lambda_2 = 0,0004990$$

$$\lambda_3 = 0,0055631$$

3. Obliczenie częstości drgań własnych:

$$\omega = \sqrt{\lambda \cdot EI}$$

$$\omega_1 = \sqrt{0,0002699 \cdot 3977000}$$

$$\omega_1 = 32,76 \frac{\text{rad}}{\text{s}}$$

$$\omega_2 = \sqrt{0,0004990 \cdot 3977000}$$

$$\omega_2 = 44,55 \frac{\text{rad}}{\text{s}}$$

$$\omega_3 = \sqrt{0,0055631 \cdot 3977000}$$

$$\omega_3 = 148,74 \frac{\text{rad}}{\text{s}}$$

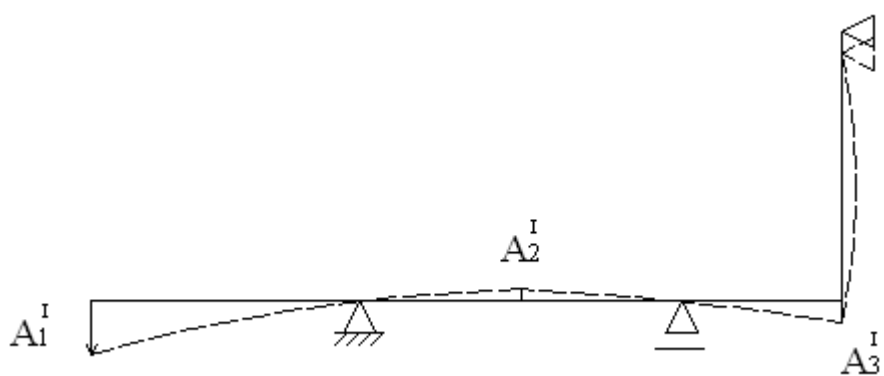
4. Obliczenie postaci drgań własnych:

- I postać drgań własnych:

- $\lambda_1 = 0,0002699$
- $A_1^I = 1,0$

$$\begin{cases} A_1(1 - 3516,8 \cdot \lambda) + 540,0 \cdot A_2 \cdot \lambda - 667,5 \cdot A_3 \cdot \lambda = 0 \\ 320,0 \cdot A_1 \cdot \lambda + A_2(1 - 252,558 \cdot \lambda) + 298,5 \cdot A_3 \cdot \lambda = 0 \end{cases}$$

$$\begin{cases} A_3^I = 0,1944 \\ A_2^I = -0,1094 \end{cases}$$

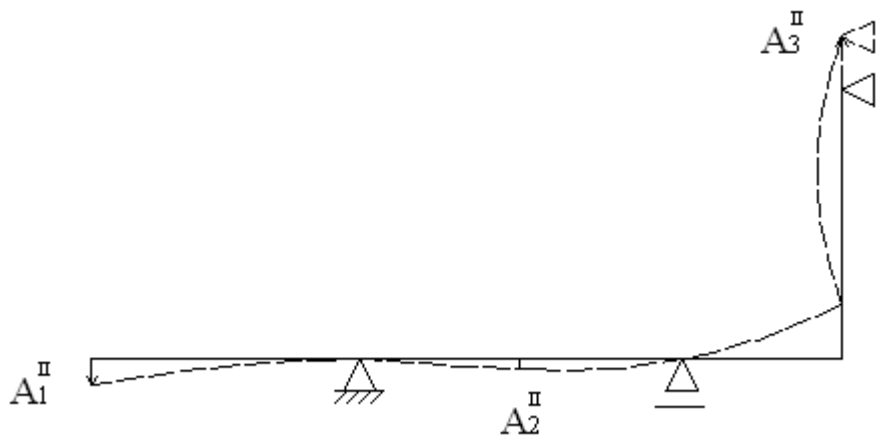


- II postać drgań własnych:

- $\lambda_2 = 0,0004990$
- $A_1^{II} = 1,0$

$$\begin{cases} A_1(1 - 3516,8 \cdot \lambda) + 540,0 \cdot A_2 \cdot \lambda - 667,5 \cdot A_3 \cdot \lambda = 0 \\ 320,0 \cdot A_1 \cdot \lambda + A_2(1 - 252,558 \cdot \lambda) + 298,5 \cdot A_3 \cdot \lambda = 0 \end{cases}$$

$$\begin{cases} A_3^{II} = -2,1218 \\ A_2^{II} = 0,17893 \end{cases}$$

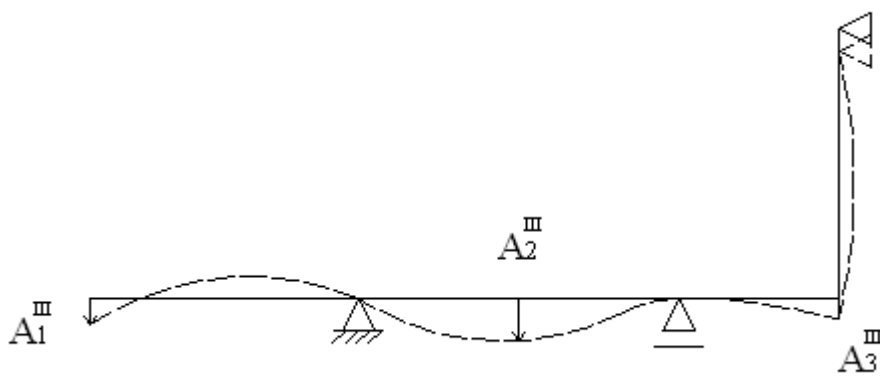


- III postać drgań własnych:

$$\begin{aligned} - \lambda_3 &= 0,005563 \\ - A_1^{\text{III}} &= 1,0 \end{aligned}$$

$$\begin{cases} A_1(1 - 3516,8 \cdot \lambda) + 540,0 \cdot A_2 \cdot \lambda - 667,5 \cdot A_3 \cdot \lambda = 0 \\ 320,0 \cdot A_1 \cdot \lambda + A_2(1 - 252,558 \cdot \lambda) + 298,5 \cdot A_3 \cdot \lambda = 0 \end{cases}$$

$$\begin{cases} A_3^{\text{III}} = 0,6231 \\ A_2^{\text{III}} = 6,9499 \end{cases}$$



5. Sprawdzenie ortogonalności drgań:

- I para drgań:

$$A_1^{\text{I}} \cdot A_1^{\text{II}} \cdot m_1 + A_2^{\text{I}} \cdot A_2^{\text{II}} \cdot m_3 + A_3^{\text{I}} \cdot A_3^{\text{II}} \cdot (m_1 + m_2) = 0$$

$$1,0 \cdot 1,0 \cdot 320,0 + (-0,1094768) \cdot 0,17893497 \cdot 540,0 + 0,1944367 \cdot (-2,12183426) \cdot 750,0 = 0$$

$$\mathbf{- 0,000021676 \cong 0}$$

- II para drgań:

$$A_1^{\text{II}} \cdot A_1^{\text{III}} \cdot m_1 + A_2^{\text{II}} \cdot A_2^{\text{III}} \cdot m_3 + A_3^{\text{II}} \cdot A_3^{\text{III}} \cdot (m_1 + m_2) = 0$$

$$1,0 \cdot 1,0 \cdot 320,0 + 0,17893497 \cdot 6,94989563 \cdot 540,0 + (-2,12183426) \cdot 0,62306651 \cdot 750,0 = 0$$

$$\mathbf{- 0,00004268 \cong 0}$$

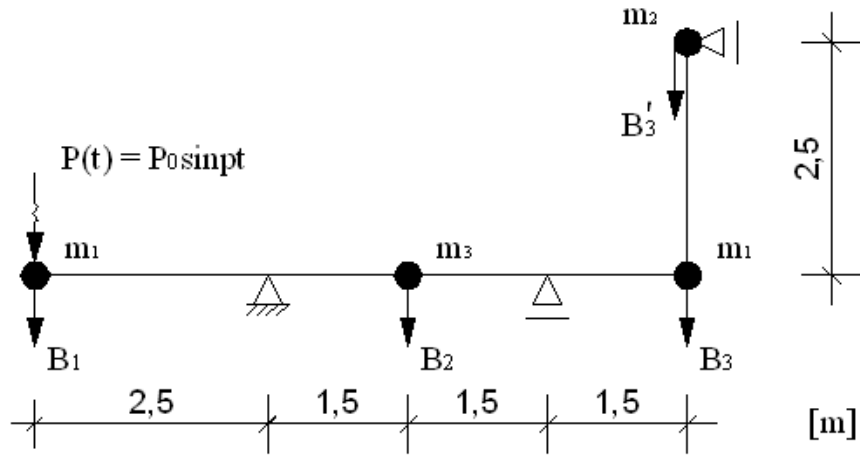
- III para drgań:

$$A_1^{\text{I}} \cdot A_1^{\text{III}} \cdot m_1 + A_2^{\text{I}} \cdot A_2^{\text{III}} \cdot m_3 + A_3^{\text{I}} \cdot A_3^{\text{III}} \cdot (m_1 + m_2) = 0$$

$$1,0 \cdot 1,0 \cdot 320,0 + (-0,1094768) \cdot 6,94989563 \cdot 540,0 + 0,1944367 \cdot 0,62306651 \cdot 750,0 = 0$$

$$\mathbf{- 0,000013236 \cong 0}$$

II. DRGANIA WYMUSZONE:



1. Dane:

- $P_0 = 62,3 \text{ kN} = 62300 \text{ N}$
- $p = 28,0 \text{ Hz} = 175,9292 \frac{\text{rad}}{\text{s}}$
- najbliższa częstość drgań własnych: $\omega_3 = 148,75 \frac{\text{rad}}{\text{s}}$
- $\eta = \frac{p}{\omega} = \frac{175,93}{148,74} = 1,18 \Rightarrow$ strefa rezonansowa ($0,75 < \eta < 1,25$)

$$\begin{aligned} q_1 &= A_1 \cdot \sin(pt) \\ q_2 &= A_2 \cdot \sin(pt) \\ q_3 &= A_3 \cdot \sin(pt) \end{aligned}$$

$$\begin{aligned} \ddot{q}_1 &= -A_1 \cdot p^2 \cdot \sin(pt) \\ \ddot{q}_2 &= -A_2 \cdot p^2 \cdot \sin(pt) \\ \ddot{q}_3 &= -A_3 \cdot p^2 \cdot \sin(pt) \end{aligned}$$

$$\begin{aligned} B_1 &= -m_1 \cdot \ddot{q}_1 \\ B_2 &= -m_3 \cdot \ddot{q}_2 \\ B_3 &= -m_1 \cdot \ddot{q}_3 \\ B'_3 &= -m_2 \cdot \ddot{q}_3 \end{aligned}$$

$$\begin{cases} q_1 = \delta_{11} \cdot B_1 + \delta_{12} \cdot B_2 + \delta_{13} \cdot (B_3 + B'_3) + \delta_{11} \cdot P(t) \\ q_2 = \delta_{21} \cdot B_1 + \delta_{22} \cdot B_2 + \delta_{23} \cdot (B_3 + B'_3) + \delta_{21} \cdot P(t) \\ q_3 = \delta_{31} \cdot B_1 + \delta_{32} \cdot B_2 + \delta_{33} \cdot (B_3 + B'_3) + \delta_{31} \cdot P(t) \end{cases}$$

$$\begin{cases} A_1 \sin(pt) = \delta_{11} \cdot 320,0 \cdot A_1 \cdot p^2 \sin(pt) + \delta_{12} \cdot 540,0 \cdot A_2 \cdot p^2 \sin(pt) + \delta_{13} \cdot (320,0 + 430,0) \cdot A_3 \cdot p^2 \sin(pt) + \delta_{11} \cdot P_0 \sin(pt) \\ A_2 \sin(pt) = \delta_{21} \cdot 320,0 \cdot A_1 \cdot p^2 \sin(pt) + \delta_{22} \cdot 540,0 \cdot A_2 \cdot p^2 \sin(pt) + \delta_{23} \cdot (320,0 + 430,0) \cdot A_3 \cdot p^2 \sin(pt) + \delta_{21} \cdot P_0 \sin(pt) \\ A_3 \sin(pt) = \delta_{31} \cdot 320,0 \cdot A_1 \cdot p^2 \sin(pt) + \delta_{32} \cdot 540,0 \cdot A_2 \cdot p^2 \sin(pt) + \delta_{33} \cdot (320,0 + 430,0) \cdot A_3 \cdot p^2 \sin(pt) + \delta_{31} \cdot P_0 \sin(pt) \end{cases}$$

$$\begin{cases} A_1 = \delta_{11} \cdot 320,0 \cdot A_1 \cdot p^2 + \delta_{12} \cdot 540,0 \cdot A_2 \cdot p^2 + \delta_{13} \cdot (320,0 + 430,0) \cdot A_3 \cdot p^2 + \delta_{11} \cdot P_0 \\ A_2 = \delta_{21} \cdot 320,0 \cdot A_1 \cdot p^2 + \delta_{22} \cdot 540,0 \cdot A_2 \cdot p^2 + \delta_{23} \cdot (320,0 + 430,0) \cdot A_3 \cdot p^2 + \delta_{21} \cdot P_0 \\ A_3 = \delta_{31} \cdot 320,0 \cdot A_1 \cdot p^2 + \delta_{32} \cdot 540,0 \cdot A_2 \cdot p^2 + \delta_{33} \cdot (320,0 + 430,0) \cdot A_3 \cdot p^2 + \delta_{31} \cdot P_0 \end{cases}$$

$$\begin{cases} A_1(1 - \delta_{11} \cdot 320,0 \cdot p^2) - \delta_{12} \cdot 540,0 \cdot A_2 \cdot p^2 - \delta_{13} \cdot (320,0 + 430,0) \cdot A_3 \cdot p^2 - \delta_{11} \cdot P_0 = 0 \\ -\delta_{21} \cdot 320,0 \cdot A_1 \cdot p^2 + A_2(1 - \delta_{22} \cdot 540,0 \cdot p^2) + \delta_{23} \cdot (320,0 + 430,0) \cdot A_3 \cdot p^2 - \delta_{21} \cdot P_0 = 0 \\ -\delta_{31} \cdot 320,0 \cdot A_1 \cdot p^2 - \delta_{32} \cdot 540,0 \cdot A_2 \cdot p^2 + A_3(1 - \delta_{33} \cdot (320,0 + 430,0) \cdot p^2) - \delta_{31} \cdot P_0 = 0 \end{cases}$$

Współczynniki δ_{ik} są takie same jak dla drgań własnych (str.9)

$$\begin{cases} A_1 \left(1 - \frac{10,99}{EI} \cdot 320,0 \cdot (175,9292)^2 \right) + \frac{1,0}{EI} \cdot 540,0 \cdot A_2 \cdot (175,9292)^2 - \frac{0,89}{EI} \cdot (320,0 + 430,0) \cdot A_3 \cdot (175,9292)^2 - \frac{10,99}{EI} \cdot 62300 = 0 \\ \frac{1,0}{EI} \cdot 320,0 \cdot A_1 \cdot (175,9292)^2 + A_2 \left(1 - \frac{0,4677}{EI} \cdot 540,0 \cdot (175,9292)^2 \right) + \frac{0,398}{EI} \cdot (320,0 + 430,0) \cdot A_3 \cdot (175,9292)^2 + \frac{1,0}{EI} \cdot 62300 = 0 \\ -\frac{0,89}{EI} \cdot 320,0 \cdot A_1 \cdot (175,9292)^2 + \frac{0,398}{EI} \cdot 540,0 \cdot A_2 \cdot (175,9292)^2 + A_3 \left(1 - \frac{2,8266}{EI} \cdot (320,0 + 430,0) \cdot (175,9292)^2 \right) - \frac{0,89}{EI} \cdot 62300 = 0 \end{cases}$$

$$\begin{cases} -26,3696 \cdot A_1 + 4,2026 \cdot A_2 - 5,1948 \cdot A_3 = 0,1722 \\ 2,4904 \cdot A_1 - 0,9655 \cdot A_2 + 2,3231 \cdot A_3 = -0,01567 \\ -2,2165 \cdot A_1 + 1,6726 \cdot A_2 - 15,4986 \cdot A_3 = 0,01394 \end{cases}$$

1. Rozwiązanie układu równań – metoda wyznaczników:

$$W = \begin{vmatrix} -26,3696 & 4,2026 & -5,1948 \\ 2,4904 & -0,9655 & 2,3231 \\ -2,2165 & 1,6726 & -15,4986 \end{vmatrix} = \mathbf{422,17916}$$

$$W_1 = \begin{vmatrix} 0,1722 & 4,2026 & -5,1948 \\ -0,01567 & -0,9655 & 2,3231 \\ 0,01394 & 1,6726 & -15,4986 \end{vmatrix} = \mathbf{1,08936}$$

$$W_2 = \begin{vmatrix} -26,3696 & 0,1722 & -5,1948 \\ 2,4904 & -0,01567 & 2,3231 \\ -2,2165 & 0,01394 & -15,4986 \end{vmatrix} = \mathbf{0,20968}$$

$$W_3 = \begin{vmatrix} -26,3696 & 4,2026 & 0,1722 \\ 2,4904 & -0,9655 & -0,01567 \\ -2,2165 & 1,6726 & 0,01394 \end{vmatrix} = \mathbf{0,01262}$$

Obliczenie amplitud drgań wymuszonych:

$$A_1 = \frac{W_1}{W} = \frac{1,08936}{422,17916} = \mathbf{0,00258 \text{ m}}$$

$$A_2 = \frac{W_2}{W} = \frac{0,20968}{422,17916} = \mathbf{0,000497 \text{ m}}$$

$$A_3 = \frac{W_3}{W} = \frac{0,01262}{422,17916} = \mathbf{0,0002989 \text{ m}}$$

2. Obliczenie sił bezwładności (dla $\sin(pt) = 1$):

$$B_1 = m_1 \cdot A_1 \cdot p^2 \cdot \sin(pt)$$

$$B_1 = 320,0 \cdot 0,00258 \cdot (175,9292)^2 \cdot 1,0 = 25550,0 \text{ N}$$

$$\mathbf{B_1 = 25,55 \text{ kN}}$$

$$B_2 = m_3 \cdot A_2 \cdot p^2 \cdot \sin(pt)$$

$$B_2 = 540,0 \cdot 0,000497 \cdot (175,9292)^2 \cdot 1,0 = 8310,0 \text{ N}$$

$$B_2 = 8,31 \text{ kN}$$

$$B_3 = m_1 \cdot A_3 \cdot p^2 \cdot \sin(pt)$$

$$B_3 = 320,0 \cdot 0,00002989 \cdot (175,9292)^2 \cdot 1,0 = 296,0 \text{ N}$$

$$B_3 = 0,2960 \text{ kN}$$

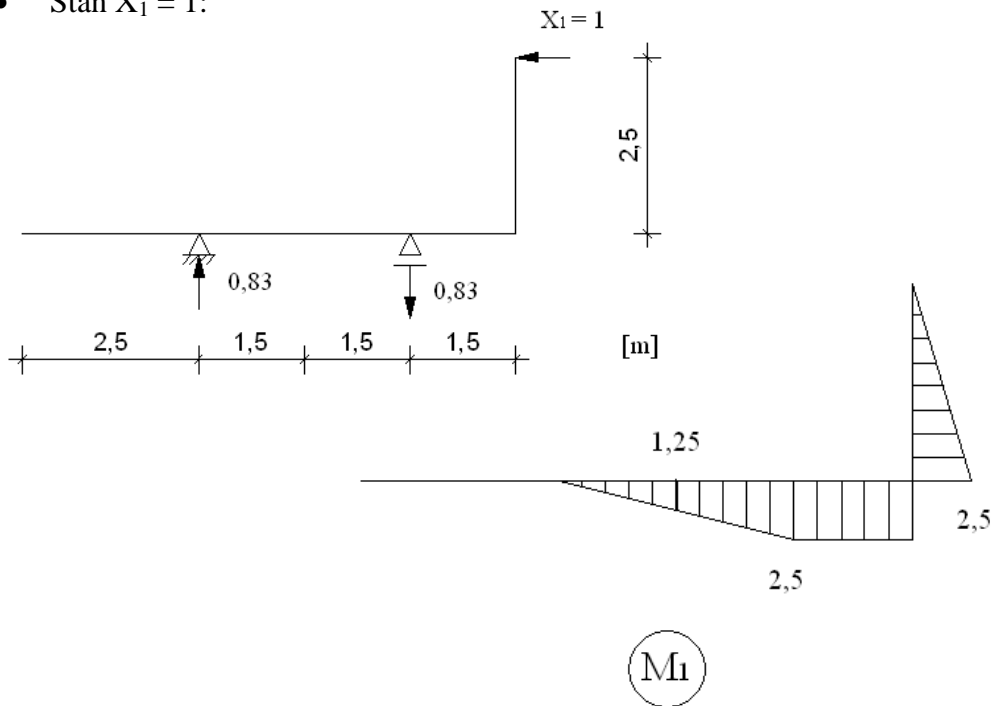
$$B'_3 = m_2 \cdot A_3 \cdot p^2 \cdot \sin(pt)$$

$$B'_3 = 430,0 \cdot 0,00002989 \cdot (175,9292)^2 \cdot 1,0 = 397,8 \text{ N}$$

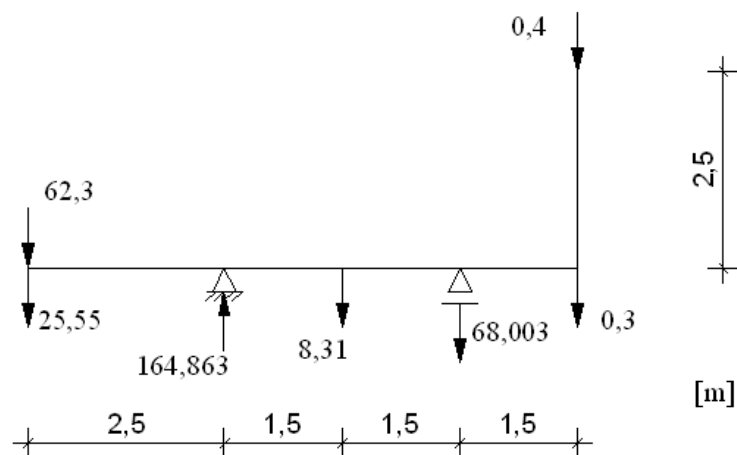
$$B'_3 = 0,3978 \text{ kN}$$

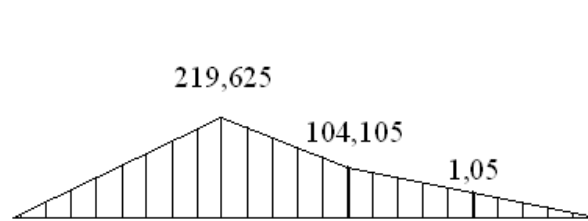
3. Obliczenie obwiedni momentów dynamicznych:

- Stan $X_1 = 1$:



- Stan „P”:



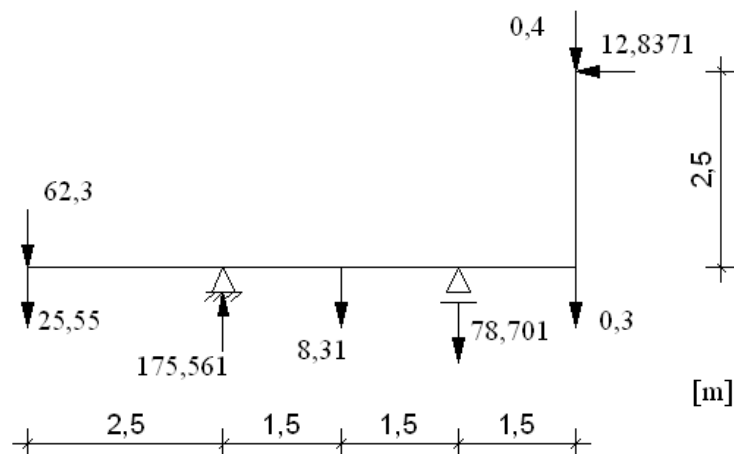


$$M_p^0$$

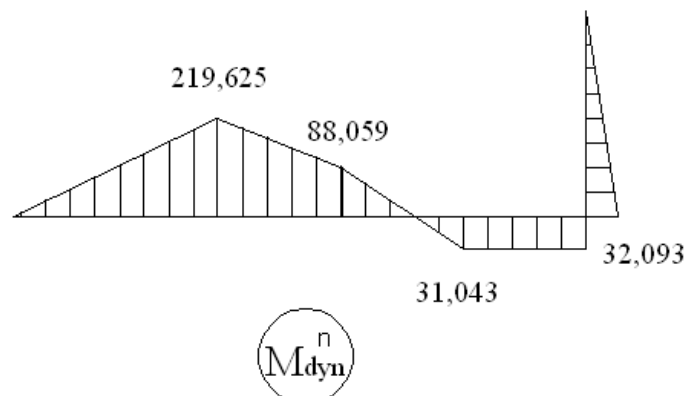
$$\delta_{11} = \frac{1}{EI} \left[\frac{1}{2} \cdot 2,5 \cdot 2,5 \cdot \frac{2}{3} \cdot 2,5 + \frac{1}{2} \cdot 3,0 \cdot 2,5 \cdot \frac{2}{3} \cdot 2,5 + 2,5 \cdot 1,5 \cdot 2,5 \right] = \frac{20,8333}{EI}$$

$$\delta_{1P} = \frac{1}{EI} \left[-\frac{1}{2} \cdot 1,25 \cdot 1,5 \cdot \left(\frac{2}{3} \cdot 104,105 + \frac{1}{3} \cdot 219,625 \right) - \frac{1}{2} \cdot 1,25 \cdot 1,5 \cdot \left(\frac{2}{3} \cdot 104,105 + \frac{1}{3} \cdot 1,05 \right) - \frac{1}{2} \cdot 2,5 \cdot 1,5 \cdot \left(\frac{2}{3} \cdot 1,05 + \frac{1}{3} \cdot 104,105 \right) - \frac{1}{2} \cdot 1,05 \cdot 1,5 \cdot 2,5 \right] = -\frac{267,4391}{EI}$$

$$X_1 = -\frac{\delta_{1P}}{\delta_{11}} = 12,8371 \text{ kN}$$

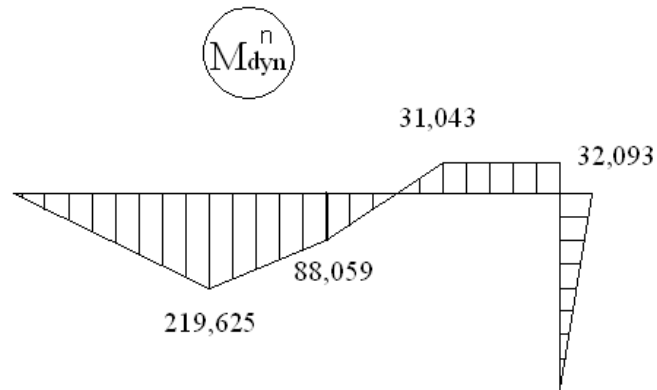


- Wykres momentów dynamicznych dla $\sin(pt) = 1$



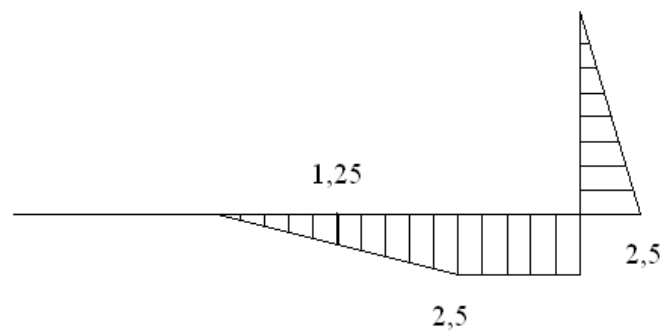
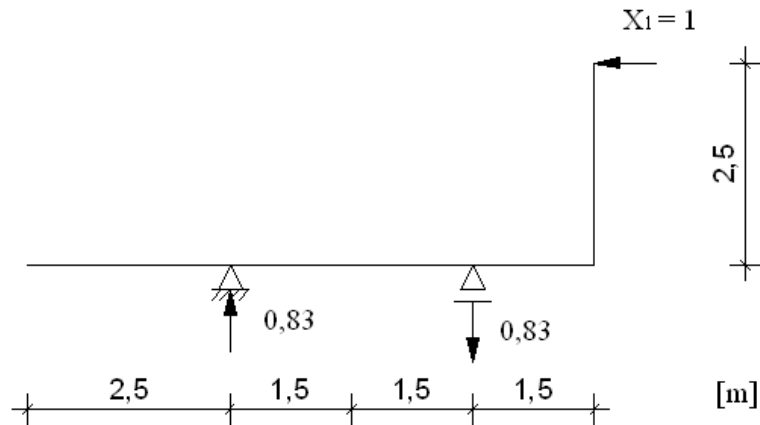
$$M_{dyn}^n$$

- Wykres momentów dynamicznych dla $\sin(pt) = -1$



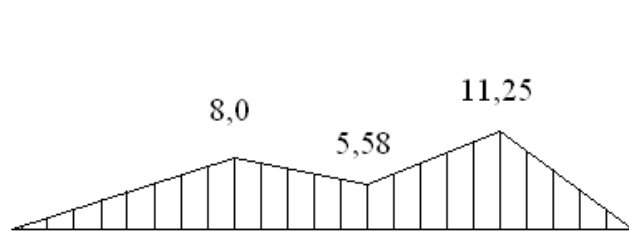
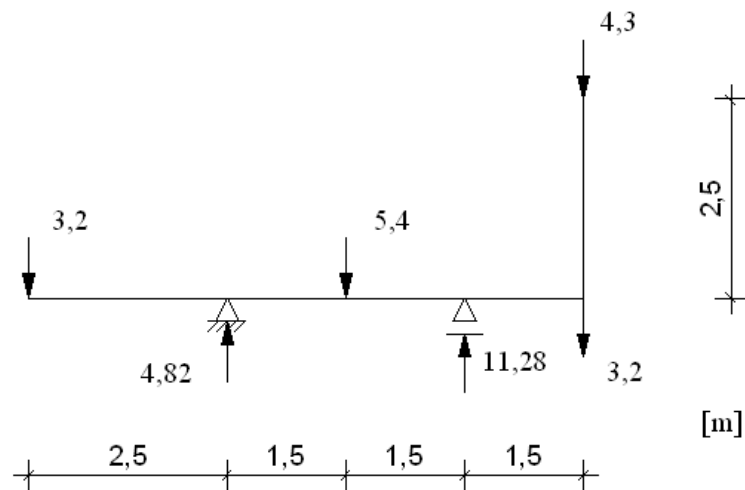
4. Obliczenie momentów statycznych od obciążenia ciężarem własnym (ciężar własny prętów pominięto):

- Stan $X_1 = 1$:



M_1

- Stan „P”:

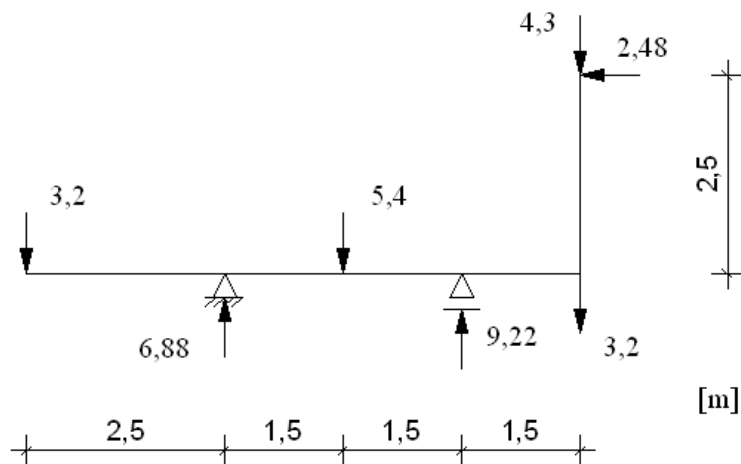


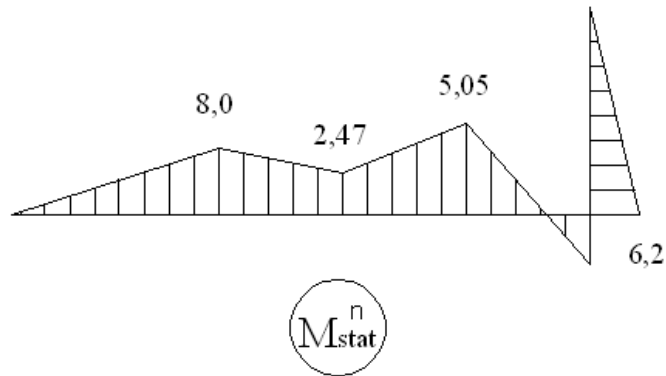
$$M_p^0$$

$$\delta_{11} = \frac{20,8333}{EI}$$

$$\delta_{1P} = \frac{1}{EI} \left[-\frac{1}{2} \cdot 1,25 \cdot 1,5 \cdot \left(\frac{2}{3} \cdot 5,58 + \frac{1}{3} \cdot 8,0 \right) - \frac{1}{2} \cdot 1,25 \cdot 1,5 \cdot \left(\frac{2}{3} \cdot 5,58 + \frac{1}{3} \cdot 11,25 \right) - \frac{1}{2} \cdot 2,5 \cdot 1,5 \cdot \left(\frac{2}{3} \cdot 11,25 + \frac{1}{3} \cdot 5,58 \right) - \frac{1}{2} \cdot 11,25 \cdot 1,5 \cdot 2,5 \right] = - \frac{51,6344}{EI}$$

$$X_1 = - \frac{\delta_{1P}}{\delta_{11}} = 2,48 \text{ kN}$$





5. Sprawdzenie maksymalnych naprężeń:

$$M_{\max} = \eta_s \cdot M_{\text{stat}} + \eta_d \cdot M_{\text{dyn}}$$

Przyjęto:

$$\eta_s = 1,2$$

$$\eta_d = 5,0$$

$$M_{\max} = 1,2 \cdot 8,0 + 5,0 \cdot 219,625$$

$$M_{\max} = 1107,725 \text{ kNm} = 110772,5 \text{ kNcm}$$

$$\sigma = \frac{M_{\max}}{W}$$

$$W = 194,0 \text{ cm}^3$$

$$\sigma = \frac{110772,5}{194,0}$$

$$\sigma = 570,9923 \frac{\text{kN}}{\text{cm}^2}$$

$$\sigma = 5709,923 \text{ MPa} > \sigma_{\text{dop}} = 215,0 \text{ MPa}$$

Przekrój nie spełnia warunku wytrzymałościowego.